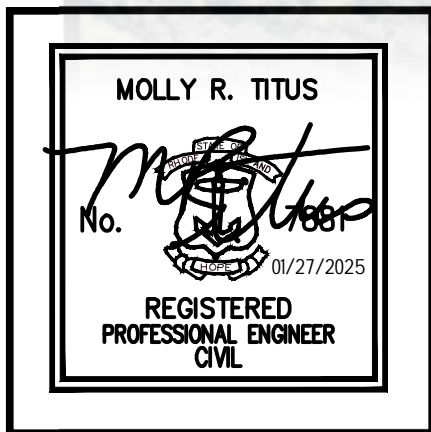




Stormwater Management Report



Saugatucket Acres

Located in South Kingstown, Rhode Island

Applicant: JAE Mills, LLC

01-27-2025

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Executive Summary

On behalf of the Client, we are submitting drainage calculations for the proposed development at 176 Saugatucket Road in South Kingstown. The site is located on Assessors' Plat 42 Lot 9. The site exists today with a single residence and contains wetlands on the southern and eastern side of the property. The client proposes to demolish the existing home, barn, and driveway, and then divide the site into five single-family lots with a shared driveway. The proposed lots will be serviced by on-site wastewater treatment systems and public water.

The post development stormwater will be treated for water quality using Best Management Practices (BMPs). The Site has been designed to meet the Rhode Island Stormwater Design and Installation Standards Manual (RISDISM). Site constraints include wetlands to the east and south, and high groundwater tables.

To mitigate post development flows on site, a series of drywells, swales are utilized to convey runoff to infiltration basins. The infiltration systems are designed to control runoff for the 2 through 100-year storm events. The drywells and water quality infiltration areas are designed as water quality BMPs. These will remove 85% or more of TSS (total suspended solids) generated by the proposed roofs and driveways.

This report details how the site will show no net increase in stormwater runoff from pre-development to post development conditions, and how the proposed BMPs will provide water quality treatment for stormwater runoff.

Pre-development Conditions versus Post Development Conditions Flow Rates for each watershed are summarized below:

| Subwatershed (design point) | 1-yr Peak Flow | | 2-yr Peak Flow | | 10-yr Peak Flow | | 25-yr Peak Flow | | 100-yr Peak Flow | |
|--------------------------------|-------------------|------|-------------------|------|--------------------|------|--------------------|------|---------------------|-------|
| | Pre | Post | Pre | Post | Pre | Post | Pre | Post | Pre | Post |
| DP-1: Saugatucket Road | 0.07 | 0.09 | 0.11 | 0.13 | 0.23 | 0.25 | 0.34 | 0.35 | 0.55 | 0.54 |
| DP-2: Wetland A | 1.67 | 1.47 | 2.67 | 2.10 | 6.52 | 4.88 | 9.80 | 8.90 | 16.87 | 16.52 |
| Totals: | 1.74 | 1.56 | 2.78 | 2.23 | 6.75 | 5.13 | 10.14 | 9.25 | 17.42 | 17.06 |

All flows in cubic feet per second (cfs)

APPENDIX A: STORMWATER MANAGEMENT PLAN CHECKLIST AND LID PLANNING REPORT – STORMWATER DESIGN SUMMARY

| | |
|---|-------------------------|
| PROJECT NAME Saugatucket Acres | (RIDEM USE ONLY) |
| TOWN South Kingstown | STW/WQC File #: |
| BRIEF PROJECT DESCRIPTION: 5 lot residential subdivision with shared access drive, public water, and private OWTS | Date Received: |

Stormwater Management Plan (SMP) Elements – Minimum Standards

When submitting a SMP,¹ submit **four separately bound** documents: Appendix A Checklist; Stormwater Site Planning, Analysis and Design Report with Plan Set/Drawings; Soil Erosion and Sediment Control (SESC) Plan, and Post Construction Operations and Maintenance (O&M) Plan. Please refer to [Suggestions to Promote Brevity](#).

Note: All stormwater construction projects **must create** a Stormwater Management Plan (SMP). However, not every element listed below is required per the [RIDEM Stormwater Rules](#) and the [RIPDES Construction General Permit \(CGP\)](#). This checklist will help identify the required elements to be submitted with an Application for Stormwater Construction Permit & Water Quality Certification.

PART 1. PROJECT AND SITE INFORMATION

PROJECT TYPE (Check all that apply)

| | | | | |
|---|-------------------------------------|----------------------------------|-----------------------------------|--------------------------------------|
| <input checked="" type="checkbox"/> Residential | <input type="checkbox"/> Commercial | <input type="checkbox"/> Federal | <input type="checkbox"/> Retrofit | <input type="checkbox"/> Restoration |
| <input type="checkbox"/> Road | <input type="checkbox"/> Utility | <input type="checkbox"/> Fill | <input type="checkbox"/> Dredge | <input type="checkbox"/> Mine |
| <input type="checkbox"/> Other (specify): | | | | |

SITE INFORMATION

Vicinity Map

INITIAL DISCHARGE LOCATION(S): The WQv discharges to: (You may choose more than one answer if several discharge points are associated with the project.)

| | | |
|---|--|--|
| <input type="checkbox"/> Groundwater | <input type="checkbox"/> Surface Water | <input type="checkbox"/> MS4 |
| <input type="checkbox"/> GAA | <input type="checkbox"/> Isolated Wetland | <input type="checkbox"/> RIDOT |
| <input checked="" type="checkbox"/> GA | <input type="checkbox"/> Named Waterbody | <input type="checkbox"/> RIDOT Alteration Permit is Approved |
| <input type="checkbox"/> GB | <input checked="" type="checkbox"/> Unnamed Waterbody Connected to Named Waterbody | <input type="checkbox"/> Town |
| | | <input type="checkbox"/> Other (specify): |

ULTIMATE RECEIVING WATERBODY LOCATION(S): Include pertinent information that applies to both WQv and flow from larger storm events including overflows. Choose all that apply, and repeat table for each waterbody.

| | |
|---|--|
| <input type="checkbox"/> Groundwater or Disconnected Wetland | <input type="checkbox"/> SRWP |
| <input checked="" type="checkbox"/> Waterbody Name: Indian Run Brook | <input type="checkbox"/> Coldwater <input checked="" type="checkbox"/> Warmwater <input type="checkbox"/> Unassessed |
| <input checked="" type="checkbox"/> Waterbody ID: RI10010045R-02 | <input type="checkbox"/> 4 th order stream of pond 50 acres or more |
| <input checked="" type="checkbox"/> TMDL for: Fecal Coliform, Copper, Zinc | <input type="checkbox"/> Watershed of flood prone river (e.g., Pocasset River) |
| <input type="checkbox"/> Contributes to a priority outfall listed in the TMDL | <input type="checkbox"/> Contributes stormwater to a public beach |
| <input checked="" type="checkbox"/> 303(d) list – Impairment(s) for: Fecal Coliform, Copper, Zinc | <input type="checkbox"/> Contributes to shellfishing grounds |

¹ Applications for a Construction General Permit that do not require any other permits from RIDEM and will disturb less than 5 acres over the entire course of the project do not need to submit a SMP. The Appendix A checklist must still be submitted.

| | | |
|---|----------------------|---|
| PROJECT HISTORY | | |
| <input type="checkbox"/> RIDEM Pre- Application Meeting | Meeting Date: | <input type="checkbox"/> Minutes Attached |
| <input type="checkbox"/> Municipal Master Plan Approval | Approval Date: | <input type="checkbox"/> Minutes Attached |
| <input type="checkbox"/> Subdivision Suitability Required | Approval #: | |
| <input type="checkbox"/> Previous Enforcement Action has been taken on the property | Enforcement #: | |
| FLOODPLAIN & FLOODWAY See Guidance Pertaining to Floodplain and Floodways | | |
| <input type="checkbox"/> Riverine 100-year floodplain: FEMA FLOODPLAIN FIRMETTE has been reviewed and the 100-year floodplain is on site | | |
| <input checked="" type="checkbox"/> Delineated from FEMA Maps: 44009C0203K and 44009C024K | | |
| NOTE: Per Rule 250-RICR-150-10-8-1.1(B)(5)(d)(3), provide volumetric floodplain compensation calculations for cut and fill/displacement calculated by qualified professional | | |
| <input type="checkbox"/> Calculated by Professional Engineer | | |
| <input type="checkbox"/> Calculations are provided for cut vs. fill/displacement volumes proposed within the 100-year floodplain | Amount of Fill (CY): | |
| | Amount of Cut (CY): | |
| <input type="checkbox"/> Restrictions or modifications are proposed to the flow path or velocities in a floodway | | |
| <input type="checkbox"/> Floodplain storage capacity is impacted | | |
| <input checked="" type="checkbox"/> Project area is not within 100-year floodplain as defined by RIDEM | | |

| | |
|--|--|
| CRMC JURISDICTION | |
| <input type="checkbox"/> CRMC Assent required | |
| <input type="checkbox"/> Property subject to a Special Area Management Plan (SAMP). If so, specify which SAMP: | |
| <input type="checkbox"/> Sea level rise mitigation has been designed into this project | |

| | | |
|---|--|-----------------------|
| LUHPPL IDENTIFICATION - MINIMUM STANDARD 8: | | |
| 1. OFFICE OF Land Revitalization and Sustainable Materials Management (OLRSMM) | | |
| <input type="checkbox"/> Known or suspected releases of HAZARDOUS MATERIAL are present at the site (Hazardous Material is defined in Rule 1.4(A)(33) of 250-140-30-1 of the RIDEM Rules and Regulations for Investigation and Remediation of Hazardous Materials (the Remediation Regulations)) | | RIDEM CONTACT: |
| <input type="checkbox"/> Known or suspected releases of PETROLEUM PRODUCT are present at the site (Petroleum Product as defined in Rule 1.5(A)(84) of 250-140-25-1 of the RIDEM Rules and Regulations for Underground Storage Facilities Used for Regulated Substances and Hazardous Materials) | | |
| <input type="checkbox"/> This site is identified on the RIDEM Environmental Resources Map as one of the following regulated facilities | | SITE ID#: |
| <input type="checkbox"/> CERCLIS/Superfund (NPL) | | |
| <input type="checkbox"/> State Hazardous Waste Site (SHWS) | | |
| <input type="checkbox"/> Environmental Land Usage Restriction (ELUR) | | |
| <input type="checkbox"/> Leaking Underground Storage Tank (LUST) | | |
| <input type="checkbox"/> Closed Landfill | | |
| Note: If any boxes in 1 above are checked, the applicant must contact the RIDEM OLRSM Project Manager associated with the Site to determine if subsurface infiltration of stormwater is allowable for the project. Indicate if the infiltration corresponds to "Red," "Yellow" or "Green" as described in Section 3.2.8 of the RISDISM Guidance (Subsurface Contamination Guidance). Also, note and reference approval in PART 3, Minimum Standard 2: Groundwater Recharge/Infiltration. | | |
| 2. PER MINIMUM STANDARD 8 of RICR 8.14.C.1-6 "LUHPPLS," THE SITE IS/HAS: | | |
| <input type="checkbox"/> Industrial Site with RIPDES MSGP, except where No Exposure Certification exists. http://www.dem.ri.gov/programs/water/permits/ripdes/stormwater/status.php | | |
| <input type="checkbox"/> Auto Fueling Facility (e.g., gas station) | | |
| <input type="checkbox"/> Exterior Vehicles Service, Maintenance, or Equipment Cleaning Area | | |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| | | |
|--|---|------------------------|
| <input type="checkbox"/> | Road Salt Storage and Loading Areas (exposed to rainwater) | |
| <input type="checkbox"/> | Outdoor Storage and Loading/Unloading of Hazardous Substances | |
| 3. STORMWATER INDUSTRIAL PERMITTING | | |
| <input type="checkbox"/> | The site is associated with existing or proposed activities that are considered Land Uses with Higher Potential Pollutant Loads (LUHPPLS) (see RICR 8.14.C) | Activities: Sector: |
| <input type="checkbox"/> | Construction is proposed on a site that is subject to THE MULTI-SECTOR GENERAL PERMIT (MSGP) UNDER RULE 31(B)15 OF THE RIPDES REGULATIONS. | MSGP permit # |
| <input type="checkbox"/> | Additional stormwater treatment is required by the MSGP Explain: | |

| REDEVELOPMENT STANDARD – MINIMUM STANDARD 6 | | |
|--|---|--|
| <input type="checkbox"/> Pre Construction Impervious Area | | |
| <input type="checkbox"/> | Total Pre-Construction Impervious Area (TIA) = 0.128 ac | |
| <input type="checkbox"/> | Total Site Area (TSA) = 9.376 ac | |
| <input type="checkbox"/> | Jurisdictional Wetlands (JW) = 5.798 ac | |
| <input type="checkbox"/> | Conservation Land (CL) = 0.0 ac | |
| <input type="checkbox"/> Calculate the Site Size (defined as contiguous properties under same ownership) | | |
| <input type="checkbox"/> | Site Size (SS) = (TSA) – (JW) – (CL) = 3.578 ac | |
| <input type="checkbox"/> | (TIA) / (SS) = 0.035 | <input type="checkbox"/> (TIA) / (SS) >0.4? No |
| <input type="checkbox"/> YES, Redevelopment | | |

PART 2. LOW IMPACT DEVELOPMENT ASSESSMENT – MINIMUM STANDARD 1
(NOT REQUIRED FOR REDEVELOPMENT OR RETROFITS)
This section may be deleted if not required.

| | |
|---|--|
| <p>Note: A written description must be provided specifying why each method is not being used or is not applicable at the Site. Appropriate answers may include:</p> <ul style="list-style-type: none"> • Town requires ... (state the specific local requirement) • Meets Town’s dimensional requirement of ... • Not practical for site because ... • Applying for waiver/variance to achieve this (pending/approved/denied) • Applying for wavier/variance to seek relief from this (pending/approved/denied) | |
| <p>A) PRESERVATION OF UNDISTURBED AREAS, BUFFERS, AND FLOODPLAINS</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Sensitive resource areas and site constraints are identified (required) <input checked="" type="checkbox"/> Local development regulations have been reviewed (required) <input checked="" type="checkbox"/> All vegetated buffers and coastal and freshwater wetlands will be protected during and after construction <input type="checkbox"/> Conservation Development or another site design technique has been incorporated to protect open space and pre-development hydrology. Note: If Conservation Development has been used, check box and skip to Subpart C <input checked="" type="checkbox"/> As much natural vegetation and pre-development hydrology as possible has been maintained | <p>IF NOT IMPLEMENTED, EXPLAIN HERE</p> |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| | |
|---|---|
| <p>B) LOCATE DEVELOPMENT IN LESS SENSITIVE AREAS AND WORK WITH THE NATURAL LANDSCAPE CONDITIONS, HYDROLOGY, AND SOILS</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Development sites and building envelopes have been appropriately distanced from wetlands and waterbodies <input type="checkbox"/> Development and stormwater systems have been located in areas with greatest infiltration capacity (e.g., soil groups A and B) <input type="checkbox"/> Plans show measures to prevent soil compaction in areas designated as Qualified Pervious Areas (QPA's) <input checked="" type="checkbox"/> Development sites and building envelopes have been positioned outside of floodplains <input checked="" type="checkbox"/> Site design positions buildings, roadways and parking areas in a manner that avoids impacts to surface water features <input checked="" type="checkbox"/> Development sites and building envelopes have been located to minimize impacts to steep slopes ($\geq 15\%$) <input type="checkbox"/> Other (describe): | <p>The entire site has soils with HSG C.</p> <p>The potential use of QPAs were evaluated, but due to the limited space and the size of the houses, drywells were determined to be more appropriate.</p> |
| <p>C) MINIMIZE CLEARING AND GRADING</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Site clearing has been restricted to <u>minimum area needed</u> for building footprints, development activities, construction access, and safety. <input checked="" type="checkbox"/> Site has been designed to position buildings, roadways, and parking areas in a manner that minimizes grading (cut and fill quantities) <input checked="" type="checkbox"/> Protection for stands of trees and individual trees and their root zones to be preserved has been specified, and such protection extends at least to the tree canopy drip line(s) <input checked="" type="checkbox"/> Plan notes specify that public trees removed or damaged during construction shall be replaced with equivalent | |
| <p>D) REDUCE IMPERVIOUS COVER</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Reduced roadway widths (≤ 22 feet for ADT ≤ 400; ≤ 26 feet for ADT 400 - 2,000) <input checked="" type="checkbox"/> Reduced driveway areas (length minimized via reduced ROW width (≤ 45 ft.) and/or reduced (or absolute minimum) front yard setback; width minimized to ≤ 9 ft. wide one lane; ≤ 18 ft. wide two lanes; shared driveways; pervious surface) <input type="checkbox"/> Reduced building footprint: Explain approach: <input checked="" type="checkbox"/> Reduced sidewalk area (≤ 4 ft. wide; one side of the street; unpaved path; pervious surface) <input checked="" type="checkbox"/> Reduced cul-de-sacs (radius < 45 ft; vegetated island; alternative turn-around) <input checked="" type="checkbox"/> Reduced parking lot area: Explain approach <input type="checkbox"/> Use of pervious surfaces for driveways, sidewalks, parking areas/overflow parking areas, etc. <input checked="" type="checkbox"/> Minimized impervious surfaces (project meets or is less than maximum specified by Zoning Ordinance) <input type="checkbox"/> Other (describe): | <p>Impervious areas were minimized to the maximum extent practicable. A shared driveway is proposed rather than a ROW. No sidewalks, parking lots, or cul-de-sacs are proposed.</p> <p>The use of pervious pavement was examined as a BMP option. However, due to the high GWTs, the amount of fill that would be required was not practical.</p> |
| <p>E) DISCONNECT IMPERVIOUS AREA</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Impervious surfaces have been disconnected, and runoff has been diverted to QPAs to the maximum extent possible <input checked="" type="checkbox"/> Residential street edges allow side-of-the-road drainage into vegetated open swales <input type="checkbox"/> Parking lot landscaping breaks up impervious expanse AND accepts runoff <input type="checkbox"/> Other (describe): | <p>No parking lots are proposed. No closed drainage system is proposed. The proposed grading across the driveways will runoff in a similar way as it does today and reach Pond Complex A via overland flow.</p> |
| <p>F) MITIGATE RUNOFF AT THE POINT OF GENERATION</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Small-scale BMPs have been designated to treat runoff as close as possible to the source | |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| | |
|---|---|
| <p>G) PROVIDE LOW-MAINTENANCE NATIVE VEGETATION</p> <ul style="list-style-type: none"> <input checked="" type="checkbox"/> Low-maintenance landscaping has been proposed using native species and cultivars <input checked="" type="checkbox"/> Plantings of native trees and shrubs in areas previously cleared of native vegetation are shown on site plan <input checked="" type="checkbox"/> Lawn areas have been limited/minimized, and yards have been kept undisturbed to the maximum extent practicable on residential lots | |
| <p>H) RESTORE STREAMS/WETLANDS</p> <ul style="list-style-type: none"> <input type="checkbox"/> Historic drainage patterns have been restored by removing closed drainage systems, daylighting buried streams, and/or restoring degraded stream channels and/or wetlands <input type="checkbox"/> Removal of invasive species <input type="checkbox"/> Other | <p>No invasive species observed. No closed drainage system is proposed.</p> |

PART 3. SUMMARY OF REMAINING STANDARDS

| GROUNDWATER RECHARGE – MINIMUM STANDARD 2 | | |
|--|-------------------------------------|--|
| YES | NO | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | The project has been designed to meet the groundwater recharge standard. |
| <input type="checkbox"/> | <input type="checkbox"/> | If “No,” the justification for groundwater recharge criterion waiver has been explained in the Narrative (e.g., threat of groundwater contamination or physical limitation), if applicable (see RICR 8.8.D); |
| <input type="checkbox"/> | <input type="checkbox"/> | Your waiver request has been explained in the Narrative, if applicable. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Is this site identified as a Regulated Facility in Part 1, Minimum Standard 8: LUHPPL Identification? |
| <input type="checkbox"/> | <input type="checkbox"/> | If “Yes,” has approval for infiltration by the OLRSM Site Project Manager, per Part 1, Minimum Standard 8, been requested? |

TABLE 2-1: Summary of Recharge (see RISDISM Section 3.3.2)
(Add or Subtract Rows as Necessary)

| Design Point | Impervious Area Treated (sq ft) | Total Re_v Required (cu ft) | LID Stormwater Credits (see RISDISM Section 4.6.1) | Recharge Required by Remaining BMPs (cu ft) | Recharge Provided by BMPs (cu ft) |
|---------------------|--|--|--|--|--|
| | | | Portion of Re_v directed to a QPA (cu ft) | | |
| DP-1: | 131 | 3 | 0 | 3 | 0 |
| DP-2: | 24,394 | 508 | 0 | 508 | 2,134 |
| TOTALS: | 24,524 | 511 | 0 | 511 | 2,134 |

Notes:

- Only BMPs listed in RISDISM Table 3-5 “List of BMPs Acceptable for Recharge” may be used to meet the recharge requirement.
- Recharge requirement must be satisfied for each waterbody ID.

Indicate where the pertinent calculations and/or information for the above items are provided (i.e., name of report/document, page numbers, appendices, etc.):

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| WATER QUALITY – MINIMUM STANDARD 3 | | |
|-------------------------------------|-------------------------------------|---|
| YES | NO | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does this project meet or exceed the required water quality volume WQv (see RICR 8.9.E-I)? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Is the proposed final impervious cover greater than 20% of the disturbed area (see RICR 8.9.E-I)? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | If “Yes,” either the Modified Curve Number Method or the Split Pervious/Impervious method in Hydro-CAD was used to calculate WQv; or, |
| <input type="checkbox"/> | <input type="checkbox"/> | If “Yes,” either TR-55 or TR-20 was used to calculate WQv; and, |
| <input type="checkbox"/> | <input type="checkbox"/> | If “No,” the project meets the minimum WQv of 0.2 watershed inches over the entire disturbed area. |
| <input type="checkbox"/> | <input type="checkbox"/> | Not Applicable |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does this project meet or exceed the ability to treat required water quality flow WQf (see RICR 8.9.I.1-3)? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does this project propose an increase of impervious cover to a receiving water body with impairments? If “Yes,” please indicate below the method that was used to address the water quality requirements of no further degradation to a low-quality water. Fully infiltrating the WQ storm. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | RICR 8.36. A Pollutant Loading Analysis is needed and has been completed. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | The Water Quality Guidance Document (Water Quality Goals and Pollutant Loading Analysis Guidance for Discharges to Impaired Waters) has been followed as applicable. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | BMPs are proposed that are on the approved technology list . If “Yes,” please provide all required worksheets from the manufacturer. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Additional pollutant-specific requirements and/or pollutant removal efficiencies are applicable to the site as the result of a TMDL, SAMP, or other watershed-specific requirements. If “Yes,” please describe: TMDL for Indian Run Brook. The WQ storm has been fully infiltrated. |

| TABLE 3-1: Summary of Water Quality (see RICR 8.9) | | | | | |
|--|--|----------------------------|--|---|--|
| Design Point and WB ID | Impervious area treated (sq ft) | Total WQv Required (cu ft) | LID Stormwater Credits (see RICR 8.18) | Water Quality Treatment Remaining (cu ft) | Water Quality Provided by BMPs (cu ft) |
| | | | WQv directed to a QPA (cu ft) | | |
| DP-1: | 131 | 11 | 0 | 11 | 0 |
| DP-2: | 24,394 | 2,033 | 0 | 2,033 | 2,134 |
| TOTALS: | 24,524 | 2,044 | 0 | 2,044 | 2,134 |
| <u>Notes:</u> | | | | | |
| 1. Only BMPs listed in RICR 8.20 and 8.25 or the Approved Technologies List of BMPs is Acceptable for Water Quality treatment. | | | | | |
| 2. For each Design Point, the Water Quality Volume Standard must be met for each Waterbody ID. | | | | | |
| <input checked="" type="checkbox"/> YES | This project has met the setback requirements for each BMP. | | | | |
| <input type="checkbox"/> NO | If “No,” please explain: | | | | |
| <input type="checkbox"/> | Indicate where the pertinent calculations and/or information for the above items are provided (i.e., name of report/document, page numbers, appendices, etc.): | | | | |
| Stormwater Report | | | | | |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| CONVEYANCE AND NATURAL CHANNEL PROTECTION (RICR 8.10) – MINIMUM STANDARD 4 | | |
|---|-------------------------------------|--|
| YES | NO | |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Is this standard waived? If “Yes,” please indicate one or more of the reasons below: |
| | | <input type="checkbox"/> The project directs discharge to a large river (i.e., 4th-order stream or larger. See RISDISM Appendix I for State-wide list and map of stream orders), bodies of water >50.0 acres in surface area (i.e., lakes, ponds, reservoirs), or tidal waters. <input type="checkbox"/> The project is a small facility with impervious cover of less than or equal to 1 acre. <input type="checkbox"/> The project has a post-development peak discharge rate from the facility that is less than 2 cfs for the 1-year, 24-hour Type III design storm event (prior to any attenuation). (<u>Note</u> : LID design strategies can greatly reduce the peak discharge rate). |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Conveyance and natural channel protection for the site have been met. If “No,” explain why: |

TABLE 4-1: Summary of Channel Protection Volumes (see RICR 8.10)

| Design Point | Receiving Water Body Name | Coldwater Fishery? (Y/N) | Total CPv Required (cu ft) | Total CPv Provided (cu ft) | Average Release Rate Modeled in the 1-yr storm (cfs) |
|---|---|---------------------------------|-----------------------------------|-----------------------------------|---|
| DP-1: | Indian Run Brook | N | See below | See below | See below |
| DP-2: | Indian Run Brook Tributary | N | See below | See below | See below |
| TOTALS: | | | | | |
| <u>Note</u> : The Channel Protection Volume Standard must be met in each waterbody ID. The 1-year storm is fully infiltrated by Infiltration Pond A. therefore the channel protection requirement has been met | | | | | |
| <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO | The CPv is released at roughly a uniform rate over a 24-hour duration (see examples of sizing calculations in Appendix D of the RISDISM). | | | | |
| <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO | Do additional design restrictions apply resulting from any discharge to cold-water fisheries; If “Yes,” please indicate restrictions and solutions below. | | | | |
| <input checked="" type="checkbox"/> Indicate below where the pertinent calculations and/or information for the above items are provided (i.e., name of report/document, page numbers, appendices, etc.). Stormwater Report | | | | | |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| OVERBANK FLOOD PROTECTION (RICR 8.11) AND OTHER POTENTIAL HIGH FLOWS – MINIMUM STANDARD 5 | | |
|---|-------------------------------------|---|
| YES | NO | |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Is this standard waived? If yes, please indicate one or more of the reasons below: |
| | | <input type="checkbox"/> The project directs discharge to a large river (i.e., 4th-order stream or larger. See Appendix I for state-wide list and map of stream orders), bodies of water >50.0 acres in surface area (i.e., lakes, ponds, reservoirs), or tidal waters. <input type="checkbox"/> A Downstream Analysis (see RICR 8.11.D and E) indicates that peak discharge control would not be beneficial or would exacerbate peak flows in a downstream tributary of a particular site (e.g., through coincident peaks). |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Does the project flow to an MS4 system or subject to other stormwater requirements? If "Yes," indicate as follows: |
| | | <input type="checkbox"/> RIDOT <input type="checkbox"/> Other (specify): |
| <p>Note: The project could be approved by RIDEM but not meet RIDOT or Town standards. RIDOT's regulations indicate that post-volumes must be less than pre-volumes for the 10-yr storm at the design point entering the RIDOT system. If you have not already received approval for the discharge to an MS4, please explain below your strategy to comply with RIDEM and the MS4.</p> | | |
| | | Indicate below which model was used for your analysis. <input type="checkbox"/> TR-55 <input type="checkbox"/> TR-20 <input checked="" type="checkbox"/> HydroCAD <input type="checkbox"/> Bentley/Haestad <input type="checkbox"/> Intellisolve <input type="checkbox"/> Other (Specify): |
| YES | NO | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does the drainage design demonstrate that flows from the 100-year storm event through a BMP will safely manage and convey the 100-year storm? If "No," please explain briefly below and reference where in the application further documentation can be found (i.e., name of report/document, page numbers, appendices, etc.): |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Do off-site areas contribute to the sub-watersheds and design points? If "Yes," |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Are the areas modeled as "present condition" for both pre- and post-development analysis? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Are the off-site areas shown on the subwatershed maps? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does the drainage design confirm safe passage of the 100-year flow through the site for off-site runoff? |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Is a Downstream Analysis required (see RICR 8.11.E.1)? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Calculate the following: |
| | | <input type="checkbox"/> Area of disturbance within the sub-watershed (areas): 3.248 ac |
| | | <input type="checkbox"/> Impervious cover (%): 32.6% |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Is a dam breach analysis required (earthen embankments over six (6) feet in height, or a capacity of 15 acre-feet or more, and contributes to a significant or high hazard dam)? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does this project meet the overbank flood protection standard? |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| Table 5-1 Hydraulic Analysis Summary | | | | | | | | |
|---|----------------------------|------------|-------------------------|------------|--------------------------|--|---------------------------|------------|
| Subwatershed (Design Point) | 1.2" Peak Flow (cfs) ** | | 1-yr Peak Flow (cfs) | | 10-yr Peak Flow (cfs) | | 100-yr Peak Flow (cfs) | |
| | Pre (cfs) | Post (cfs) | Pre (cfs) | Post (cfs) | Pre (cfs) | Post (cfs) | Pre (cfs) | Post (cfs) |
| DP-1: | 0.01 | 0.02 | 0.07 | 0.09 | 0.23 | 0.25 | 0.55 | 0.54 |
| DP-2: | 0.30 | 0.24 | 1.67 | 1.47 | 6.52 | 4.88 | 16.87 | 16.52 |
| TOTALS: | 0.31 | 0.26 | 1.74 | 1.56 | 6.75 | 5.13 | 17.42 | 17.06 |
| ** Utilize modified curve number method or split pervious /impervious method in HydroCAD. | | | | | | | | |
| <u>Note:</u> The hydraulic analysis must demonstrate no impact to each individual subwatershed DP unless each DP discharges to the same wetland or water resource. | | | | | | | | |
| Indicate as follows where the pertinent calculations and/or information for the items above are provided | | | | | | Name of report/document, page numbers, appendices, etc. | | |
| Existing conditions analysis for each subwatershed, including curve numbers, times of concentration, runoff rates, volumes, and water surface elevations showing methodologies used and supporting calculations. | | | | | | Stormwater report | | |
| Proposed conditions analysis for each subwatershed, including curve numbers, times of concentration, runoff rates, volumes, water surface elevations, and routing showing the methodologies used and supporting calculations. | | | | | | Stormwater report | | |
| Final sizing calculations for structural stormwater BMPs, including contributing drainage area, storage, and outlet configuration. | | | | | | Stormwater report | | |
| Stage-storage, inflow and outflow hydrographs for storage facilities (e.g., detention, retention, or infiltration facilities). | | | | | | Stormwater report | | |

| Table 5-2 Summary of Best Management Practices | | | | | | | | | | | | |
|--|------|--|------------------------|-----------------|-----------------|--------------------------|-----------------------------------|-------------|---|-----------|---|-------------------|
| BMP ID | DP # | BMP Type (e.g., bioretention, tree filter) | BMP Functions | | | | | Bypass Type | Horizontal Setback Criteria are met per RICR 8.21.B.10, 8.22.D.11, and 8.35.B.4 | | | |
| | | | Pre-Treatment (Y/N/NA) | Re _v | WQ _v | CP _v (Y/N/NA) | Overbank Flood Reduction (Y/N/NA) | | External (E) Internal (I) or NA | Yes/No | Technical Justification (Design Report page number) | Distance Provided |
| 204/ 206/ 208 | 2 | Pond Complex A (sediment forebay, WQ Infiltration, Infiltration) | Y | Y | Y | Y | Y | Internal | Yes | See Plans | See Plans | |
| | 2 | Drywells | NA | Y | Y | NA | NA | NA | Yes | See Plans | See Plans | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | TOTALS: | | | | | | | | | | |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| Table 5.3 Summary of Soils to Evaluate Each BMP | | | | | | | | | |
|--|--------|---|--------------------------------------|-----------|---------------------------|---|--|--|--|
| DP # | BMP ID | BMP Type (e.g., bioretention, tree filter) | Soils Analysis for Each BMP | | | | | | |
| | | | Test Pit ID# and Ground Elevation | | SHWT Elevation (ft) | Bottom of Practice Elevation* (ft) | Separation Distance Provided (ft) | Hydrologic Soil Group (A, B, C, D) | Exfiltration Rate Applied (in/hr) |
| | | | Primary | Secondary | | | | | |
| 2 | 206 | WQ Infiltration | 22-8 | 22-10 | 92.47 | 94.50 | 2.03 | C | 0.99 |
| 2 | 208 | Infiltration | 22-8 | 22-10 | 92.17 | 94.50 | 2.33 | C | 0.99 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | TOTALS: | | | | | | | |

* For underground infiltration systems (UICs) bottom equals bottom of stone, for surface infiltration basins bottom equals bottom of basin, for filters bottom equals interface of storage and top of filter layer

| LAND USES WITH HIGHER POTENTIAL POLLUTANTS LOADS (LUHPPLs) – MINIMUM STANDARD 8 | | | |
|--|--------------------------|-------------------------------------|--|
| YES | NO | N/A | |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | Describe any LUHPPLs identified in Part 1, Minimum Standard 8, Section 2. If not applicable, continue to Minimum Standard 9. |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | Are these activities already covered under an MSGP? If “No,” please explain if you have applied for an MSGP or intend to do so? |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | List the specific BMPs that are proposed for this project that receive stormwater from LUHPPL drainage areas. These BMP types must be listed in RISDISM Table 3-3, “Acceptable BMPs for Use at LUHPPLs.” Please list BMPs: |
| <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | Additional BMPs, or additional pretreatment BMP’s if any, that meet RIPDES MSGP requirements; Please list BMPs: |
| | | | Indicate below where the pertinent calculations and/or information for the above items are provided (i.e., name of report/document, page numbers, appendices, etc.). |

| ILLICIT DISCHARGES – MINIMUM STANDARD 9 | | | |
|--|-------------------------------------|--------------------------|--|
| Illicit discharges are defined as unpermitted discharges to Waters of the State that do not consist entirely of stormwater or uncontaminated groundwater, except for certain discharges identified in the RIPDES Phase II Stormwater General Permit. | | | |
| YES | NO | N/A | |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | Have you checked for illicit discharges? |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | Have any been found and/or corrected? If “Yes,” please identify. |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | Does your report explain preventative measures that keep non-stormwater discharges out of the Waters of the State (during and after construction)? |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| SOIL EROSION AND SEDIMENT CONTROL (SESC) – MINIMUM STANDARD 10 | | |
|---|--------------------------|---|
| YES | NO | N/A |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| | | <p>Have you included a Soil Erosion and Sediment Control Plan Set and/or Complete Construction Plan Set?</p> <p>Have you provided a separately-bound document based upon the SESC Template? If yes, proceed to Minimum Standard 11 (the following items can be assumed to be addressed).</p> <p>If “No,” include a document with your submittal that addresses the following elements of an SESC Plan:</p> |
| <input checked="" type="checkbox"/> | | Soil Erosion and Sediment Control Plan Project Narrative, including a description of how the fifteen (15) Performance Criteria have been met: |
| <input checked="" type="checkbox"/> | | Provide Natural Buffers and Maintain Existing Vegetation |
| <input checked="" type="checkbox"/> | | Minimize Area of Disturbance |
| <input checked="" type="checkbox"/> | | Minimize the Disturbance of Steep Slopes |
| <input checked="" type="checkbox"/> | | Preserve Topsoil |
| <input checked="" type="checkbox"/> | | Stabilize Soils |
| <input checked="" type="checkbox"/> | | Protect Storm Drain Inlets |
| <input checked="" type="checkbox"/> | | Protect Storm Drain Outlets |
| <input checked="" type="checkbox"/> | | Establish Temporary Controls for the Protection of Post-Construction Stormwater Control Measures |
| <input checked="" type="checkbox"/> | | Establish Perimeter Controls and Sediment Barriers |
| <input checked="" type="checkbox"/> | | Divert or Manage Run-On from Up-Gradient Areas |
| <input checked="" type="checkbox"/> | | Properly Design Constructed Stormwater Conveyance Channels |
| <input checked="" type="checkbox"/> | | Retain Sediment On-Site |
| <input checked="" type="checkbox"/> | | Control Temporary Increases in Stormwater Velocity, Volume, and Peak Flows |
| <input checked="" type="checkbox"/> | | Apply Construction Activity Pollution Prevention Control Measures |
| <input checked="" type="checkbox"/> | | Install, Inspect, and Maintain Control Measures and Take Corrective Actions |
| <input checked="" type="checkbox"/> | | Qualified SESC Plan Preparer’s Information and Certification |
| <input checked="" type="checkbox"/> | | Operator’s Information and Certification; if not known at the time of application, the Operator must certify the SESC Plan upon selection and prior to initiating site activities |
| <input checked="" type="checkbox"/> | | Description of Control Measures, such as Temporary Sediment Trapping and Conveyance Practices, including design calculations and supporting documentation, as required |

| STORMWATER MANAGEMENT SYSTEM OPERATION, MAINTENANCE, AND POLLUTION PREVENTION PLAN – MINIMUM STANDARDS 7 AND 9 | | |
|---|-------------------------------------|---|
| Operation and Maintenance Section | | |
| YES | NO | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Have you minimized all sources of pollutant contact with stormwater runoff, to the maximum extent practicable? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Have you provided a separately-bound Operation and Maintenance Plan for the site and for all of the BMPs, and does it address each element of RICR 8.17 and RISDISM Appendix C and E? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Lawn, Garden, and Landscape Management meet the requirements of RISDISM Section G.7? If “No,” why not? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Is the property owner or homeowner’s association responsible for the stormwater maintenance of all BMP’s? If “No,” you must provide a legally binding and enforceable maintenance agreement (see RISDISM Appendix E, page 26) that identifies the entity that will be responsible for maintenance of the stormwater. Indicate where this agreement can be found in your report (i.e., name of report/document, page numbers, appendices, etc.). |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Do you anticipate that you will need legal agreements related to the stormwater structures? (e.g. off-site easements, deed restrictions, covenants, or ELUR per the Remediation Regulations). If “Yes,” have you obtained them? Or please explain your plan to obtain them: |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| | | |
|-------------------------------------|-------------------------------------|---|
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Is stormwater being directed from public areas to private property? If "Yes," note the following: <u>Note:</u> This is not allowed unless a funding mechanism is in place to provide the finances for the long-term maintenance of the BMP and drainage, or a funding mechanism is demonstrated that can guarantee the long-term maintenance of a stormwater BMP by an individual homeowner. |
| Pollution Prevention Section | | |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Designated snow stockpile locations? |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Trash racks to prevent floatables, trash, and debris from discharging to Waters of the State? |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Asphalt-only based sealants? |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Pet waste stations? (<u>Note:</u> If a receiving water has a bacterial impairment, and the project involves housing units, then this could be an important part of your pollution prevention plan). |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Regular sweeping? Please describe: |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | De-icing specifications, in accordance with RISDISM Appendix G. (NOTE: If the groundwater is GAA, or this area contributes to a drinking water supply, then this could be an important part of your pollution prevention plan). |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | A prohibition of phosphate-based fertilizers? (<u>Note:</u> If the site discharges to a phosphorus impaired waterbody, then this could be an important part of your pollution prevention plan). |

PART 4. SUBWATERSHED MAPPING AND SITE-PLAN DETAILS

| Existing and Proposed Subwatershed Mapping (REQUIRED) | | |
|--|-------------------------------------|---|
| YES | NO | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Existing and proposed drainage area delineations |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Locations of all streams and drainage swales |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Drainage flow paths, mapped according to the DEM <i>Guidance for Preparation of Drainage Area Maps</i> (included in RISDISM Appendix K) |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Complete drainage area boundaries; include off-site areas in both mapping and analyses, as applicable |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Logs of borings and/or test pit investigations along with supporting soils/geotechnical report |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Mapped seasonal high-water-table test pit locations |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Mapped locations of the site-specific borings and/or test pits and soils information from the test pits at the locations of the BMPs |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Mapped locations of the BMPs, with the BMPs consistently identified on the Site Construction Plans |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Mapped bedrock outcrops adjacent to any infiltration BMP |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Soils were logged by a: |
| | <input checked="" type="checkbox"/> | DEM-licensed Class IV soil evaluator Name: Timothy Twohig |
| | <input type="checkbox"/> | RI-registered P.E. Name: |

| Subwatershed and Impervious Area Summary | | | | |
|---|--|-----------------------------------|--|--|
| Subwatershed (area to each design point) | First Receiving Water ID or MS4 | Area Disturbed (units) | Existing Impervious (units) | Proposed Impervious (units) |
| DP-1: | Indian Run Brook | 0.049 ac | 0.012 ac | 0.015 ac |
| DP-2: | Indian Run Brook Tributary | 3.201 ac | 0.305 ac | 0.740 ac |
| DP-3: | | | | |
| DP-4: | | | | |
| TOTALS: | | | | |

Stormwater Management, Design, and Installation Rules (250-RICR-150-10-8)

| Site Construction Plans (Indicate that the following applicable specifications are provided) | | |
|---|-------------------------------------|---|
| YES | NO | |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Existing and proposed plans (scale not greater than 1" = 40') with North arrow |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Existing and proposed site topography (with 1 or 2-foot contours); 10-foot contours accepted for off-site areas |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Boundaries of existing predominant vegetation and proposed limits of clearing |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Site Location clarification |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Location and field-verified boundaries of resource protection areas such as: <ul style="list-style-type: none"> ▶ freshwater and coastal wetlands, including lakes and ponds ▶ coastal shoreline features Perennial and intermittent streams, in addition to Areas Subject to Storm Flowage (ASSFs) |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | All required setbacks (e.g., buffers, water-supply wells, septic systems) |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Representative cross-section and profile drawings, and notes and details of structural stormwater management practices and conveyances (i.e., storm drains, open channels, swales, etc.), which include: <ul style="list-style-type: none"> ▶ Location and size of the stormwater treatment practices (type of practice, depth, area). Stormwater treatment practices (BMPs) must have labels that correspond to RISDISM Table 5-2; ▶ Design water surface elevations (applicable storms); ▶ Structural details of outlet structures, embankments, spillways, stilling basins, grade-control structures, conveyance channels, etc.; ▶ Existing and proposed structural elevations (e.g., inverts of pipes, manholes, etc.); ▶ Location of floodplain and, if applicable, floodway limits and relationship of site to upstream and downstream properties or drainage that could be affected by work in the floodplain; ▶ Planting plans for structural stormwater BMPs, including species, size, planting methods, and maintenance requirements of proposed planting |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Logs of borings and/or test pit investigations along with supporting soils/geotechnical report and corresponding water tables |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Mapping of any OLRSM-approv ed remedial actions/systems (including ELURs) |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Location of existing and proposed roads, buildings, and other structures including limits of disturbance; <ul style="list-style-type: none"> ▶ Existing and proposed utilities (e.g., water, sewer, gas, electric) and easements; ▶ Location of existing and proposed conveyance systems, such as grass channels, swales, and storm drains, and location(s) of final discharge point(s) (wetland, waterbody, etc.); ▶ Cross sections of roadways, with edge details such as curbs and sidewalks; ▶ Location and dimensions of channel modifications, such as bridge or culvert crossings |
| <input type="checkbox"/> | <input checked="" type="checkbox"/> | Locations, cross sections, and profiles of all stream or wetland crossings and their method of stabilization |

1.0 Project Description

The purpose of this report is to specify a Stormwater Management System to be implemented at the proposed Saugatucket Acres residential development at 176 Saugatucket Road in South Kingstown. The site is located on Assessors' Plat 42 Lot 9. The site exists today with a single residence and contains wetlands on the southern and eastern side of the property. Indian Run Brook, which is impaired for fecal coliform, copper and zinc, briefly crosses the southeastern property corner. The client proposes to demolish the existing home, barn, and driveway, and divide the site into five single-family lots with a shared driveway. The proposed lots will be serviced by on-site wastewater treatment systems and public water.

The stormwater quality will be improved by utilizing Best Management Practices (BMPs) as established by the RIDISM for the treatment of stormwater runoff from the proposed development. BMPs will consist of drywells, a sediment forebay, and infiltration ponds. The system has been designed to meet the RIDEM Stormwater Design and Installations Standards Manual.

2.0 Site Conditions

2.1 SOILS

There are the following soil types within the analyzed area of the Site as mapped by the NRCS USDA Soil Conservation service:

| Soil Symbol | Description | Hydrologic Group |
|-------------|---|------------------|
| BrA | Broadbrook silt loam, 0 to 3 percent slopes | C |
| RaB | Rainbow silt loam, 3 to 8 percent slopes | C |
| Se | Stissing silt loam | D |
| Sf | Stissing very stony silt loam | D |

Site specific soil evaluations can be found in Appendix A2.1.

2.2 EXISTING SITE CONDITIONS

Currently, the northern and western portions of the site have a mixture of grass and brush and contains an existing residence with a barn and driveway with access on Saugatucket Road. The southern and eastern portions of the site are predominantly wooded wetlands. Indian Run Brook, which has impairments for fecal coliform, copper and zinc, briefly crosses the southeastern property corner. The site is surrounded by residences on the north and west sides, and wetlands on the east and south sides.

Stone walls encompass the northern and western of property edges, forming topographic ridges. The site is relatively flat and generally slopes from the northwest to the southeast.

Two design points have been identified on. Design Point-1 is the roadside swale along Saugatucket Road that flows west. Stormwater from this design point continues along Saugatucket Road until it reaches a tributary of Indian Run Brook. Design Point-2 is the A-Series Wetland in the southeaster portion of the

site. Stormwater from this design point continues through the wetland until it reaches Indian Run Brook.

Stormwater onsite is not currently treated before it is discharged to the design points.

2.3 POST SITE CONDITIONS

The proposed drainage analysis uses stormwater management systems to control and treat runoff from the proposed development. The following BMP's are used on site and have been designed to include the following elements:

- Sediment Forebay
 - Pretreatment of driveways
 - 2.0' forebay depth with proposed 2:1 reinforced slopes.
 - Acts as a water quality bypass. The water quality storm is directed to the water quality infiltration basin while other storms are bypassed within sediment forebay to Infiltration Pond A.
 - Equipped with Water quality stormwater event by-pass to the water quality BMP.
 - Equipped with secondary weir for larger stormwater events to detention pond
 - Velocities < 2 ft/sec over weir from Sediment Forebay to the CPv/QP BMP.
- WQ Infiltration Pond
 - Fully infiltrates the water quality stormwater event.
- Open Channels (Swales)
 - Provide conveyance of stormwater.
- Infiltration Pond
 - All stormwater is treated before entering the stormwater basin.
 - Fully infiltrates the Channel Protection Volume (CPv).
 - Provided Overbank Flood Protection (Qp) for the 2-100 year storm events.
- Drywells
 - WQ treatment of roofs
 - Fully infiltrates the water quality storm event.

The above elements will used to meet the design standards of the Rhode Island Stormwater Design and Installation Standard.

The primary goal of increasing water quality treatment is accomplished by providing drywells, a sediment forebay, and a water quality infiltration pond. Stormwater runoff mitigation is provided through the use of the infiltration pond. While this project has not been classified as a redevelopment project, impervious areas exist onsite and currently runoff untreated to a waterbody with a TMDL and an impairment. The proposed design now fully treats all proposed impervious to the impaired waterbody and fully infiltrates the 1-year storm. By reducing post development stormwater flow rate to a level no greater than the pre-development rate, the second goal of the proposed drainage system is achieved. Any potential impacts from the proposed development on the abutting properties, wetlands and Indian Run Brook have been mitigated.

3.0 Minimum Standards

The site has been designed to meet the minimum standards as outlined in the Rhode Island Stormwater Design and Installation Standards Manual (RISDISM). The following sections outline how the site meets and exceeds the minimum required standards.

3.1 Minimum Standard 1: LID Site Planning and Design Strategies

See "Appendix A: Stormwater Management Checklist" from the RISDISM provided at the beginning of this report.

3.2 Minimum Standard 2: Groundwater Recharge

Groundwater is to be recharged per watershed based on impervious area coverage in accordance with section 3.2.2 of the RISDISM.

Groundwater recharge is determined from the following equation:

$$Re_v = 1'' * F * I / 12$$

Where:

Re_v = Groundwater Recharge Volume (cf)

F = Recharge Factor based on Hydrologic Soil Groups (HSG) (see table below)

I = Impervious Area (sf)

| HSG | Recharge Factor (F) |
|-----|---------------------|
| A | 0.60 |
| B | 0.35 |
| C | 0.25 |
| D | 0.10 |

Recharge volumes are provided through the use of house drywells and WQ Infiltration Pond A. See Table 2-1 of the Appendix A checklist for a summary of recharge values.

The required recharge volume is based on all impervious area, not just areas which are captured in the proposed BMPs.

See Appendix A3.2 for the water quality storm HydroCAD analysis. The water quality storm is calculated in HydroCAD using the 'calculate separate Pervious/Impervious runoff' option.

3.3 Minimum Standard 3: Water Quality

All stormwater is treated through an approved BMP before being discharged. This site has been designed to use drywells and a WQ Infiltration Pond to treat stormwater before being infiltrated within the infiltration basin. See the drywell and infiltration pond design sheets for water quality requirements. Indian Run Brook is the ultimate receiving waterbody for design point 1 and has a TMDL for fecal coliform, copper and zinc.

Drywells

Each roof is directed to a drywell, which fully infiltrates the water quality storm event. Drywells have been designed in HydroCAD and have been assigned an infiltration rate based on infiltration tests that have been conducted onsite. To be conservative, the infiltration rates used in the design are 1/2 of what was observed in the field. It should be noted that, to be conservative, drywells have not been included in

the HydroCAD model. Roof areas are within the subcatchments that the drywell will overtop in during larger storm events.

Water Quality Infiltration Pond

The infiltration pond has been sized using HydroCAD and an infiltration rate based on a parent material within the footprint of the BMP. The project site largely consists of silty loam and an infiltration rate was measured in the field. To be conservative, the infiltration rate used in the design is ½ of what was observed in the field. See Appendix A3.2 for the HydroCAD analysis for the water quality event. The infiltration pond has been designed to fully infiltrate the water quality event.

Pretreatment for the infiltration pond has been provided through the use of a sediment forebay. The forebay has been sized per section 6.4 of the RISDISM.

Infiltration Pond Parameters:

| BMP | Total Watershed Area (acres) | Impervious (acres) | Required Forebay Volume (cf) | Provided Forebay Volume (cf) | Required Surface Area, As (sf) | Provided Surface Area, As (sf) |
|--------|------------------------------|--------------------|------------------------------|------------------------------|--------------------------------|--------------------------------|
| Pond-A | 1.630 | 0.318 | 296 | 399 | 20 | 88 |

3.4 Minimum Standard 4: Conveyance and Natural Channel Protection

3.4.1 Drainage Network Design Parameters:

A. PIPES

- All drainage pipes are HDPE or equivalent unless otherwise noted.
- Manning's coefficient = 0.012 for HDPE Pipe
- Diameters & lengths as specified

B. STRUCTURES

- No structures are proposed

C. OPEN CHANNELS SYSTEMS (SWALES)

- All open channels systems shall be grass channels
- Manning's coefficient =0.030
- Width, depth, slope and side slopes as noted on plans.
- The 100-year design storm is utilized for the open channel design to ensure that the drainage system contains and channels water to the BMP areas as shown on the plans.

3.4.2 Channel Protection Volume:

The site has been designed to fully infiltrate the channel protection volume. The channel protection required has been met.

See table 4-1 of the Appendix A Checklist for a Summary of Channel Protection Volumes. See Appendix A3.5.4.2 for the 1-year storm event HydroCAD analysis.

3.5 Minimum Standard 5: Overbank Flood Protection & Downstream Analysis

3.5.1 Method of Analysis

USDA Soil Conservation Service Method as defined by Technical Release No. 20 (TR-20) determines Stormwater runoff rate and volume. Type III rainfall distribution is utilized. Time of concentration is

determined using Technical Release No 55 (TR-55) methodology, through the computer program *HydroCAD ver. 10.0* by HydroCAD Software Solutions LLC.

Infiltration pond soils has been modeled in HydroCAD with a 0.99 inches/hr infiltration rate, which is ½ the rate that was observed in the field. Soil evaluations and infiltration tests have been performed by DiPrete Engineering. The existing soil has a texture of predominantly silty loam.

The drainage system has been designed to mitigate all stormwater flows for the 10- and 100-year storm events. The emergency outlets have been sized to handle the 100-year storm event.

3.5.2 Design Storm

Analysis of 1-year, 10-year, 25-year, and 100-year frequency storms are included. The following 24-hour rainfall intensities are obtained from the Rhode Island Stormwater Design and Installation Standards Manual, Table 3-1 for Washington County.

| | |
|-----------|------------|
| 1 year = | 2.8 inches |
| 10 year = | 4.9 inches |
| 25 year = | 6.1 inches |
| 100 year= | 8.5 inches |

3.5.3 Design Point Breakdown

The site is analyzed as two watershed areas. In the pre-development stage, there are five subcatchments. In the post development stage, there are six subcatchments. Each watershed will demonstrate zero increase of runoff due to the proposed development. A description of each watershed and associated subcatchments are summarized as follows, for cover types see color watershed maps located in back of this report. Numbers in parentheses () indicate the HydroCAD Node Number.

Design Point 1:

Watershed one flows to Design Point- 1 (DP-1). The design point is a swale along Saugatucket Road that flows west.

In pre-development conditions there is only one watershed to Design Point-1 (12).

Pre-01 (11) contains the northwest corner of the property and Saugatucket Road. Stormwater reaches DP-1 (12) via overland flow.

In post development conditions there is one subwatershed:

Post-1 (101) collects runoff from the northwestern corner of the property and Saugatucket Road.

Below is a summary of the hydrologic parameters for the pre and post development sub-areas in Design Point-1.

| | Area (acres) | CN | Tc (min) |
|---------|--------------|----|----------|
| Pre-01 | 0.087 | 75 | 6.0 |
| Post-01 | 0.078 | 79 | 6.0 |

Design Point 2:

Watershed two flows to Design Point- 2 (DP-2). The design point is the A-Series Wetland to the south and east.

In pre-development conditions there are four watersheds to Design Point-2.

Pre-02 (21) contains the western section of the site. Stormwater reaches DP-2 (25) via overland flow.

Pre-03 (22) contains the centermost section of the site. Stormwater reaches DP-2 (25) via overland flow.

Pre-04 (23) contains the northeastern portion of the site. Stormwater reaches DP-2 (25) via overland flow through the B-Series Wetland.

Pre-05 (24) contains a small section of the site along Saugatucket and predominantly contains offsite area. Stormwater reaches DP-2 via overland flow via a swale along Saugatucket Road.

In post development conditions there are five sub watersheds:

Post-2 (201) collects runoff from the western side of the site. Stormwater reaches DP-2 via overland flow.

Post-3 (202) contains a small section of the site along Saugatucket and predominantly contains offsite area. Stormwater reaches DP-2 via overland flow via a swale along Saugatucket Road.

Post-4 (203) is the center of the site and includes the proposed driveways and most of the drywells. Stormwater reaches DP-2 via Pond Complex A (204, 206, 208). Drywells within this subcatchment fully infiltrate the water quality storm. During larger storm events, runoff from the roof areas flow overland to Pond Complex A (204, 206, 208)

Post-4 (205) is the WQ Infiltration Pond A area.

Post-5 (207) is the Infiltration Pond A area.

3.5.4 Q_p BMP Calculations

The section includes calculations for each Q_p BMP for the site. Calculations are for Emergency Outlet Calculations.

The emergency outlet has been sized to safely pass the 100-year storm and beyond without erosion or overtopping the embankment. For this analysis, the infiltration pond was assumed to have no proposed infiltration and only the weir functioning. Under normal conditions, the basin will have a minimum of one foot of freeboard.

| Basin | Q(cfs) | V (ft/s) | Top of Basin | Flood Elevation |
|--------|--------|----------|--------------|-----------------|
| Pond A | 9.01 | 2.63 | 97.00 | 96.44 |

The velocity over the spillway is less than 3 ft/s thus no erosion will take place on the embankment or downstream. The basin maintains freeboard even with no infiltration and the 100-year storm flowing over the embankment. See attached HydroCAD.

3.5.5 Downstream Analysis

A downstream analysis is required under the following conditions:

| Area of Disturbance (Acres) | Impervious Cover (%) |
|-----------------------------|----------------------|
| >5 to 10 | >75 |
| >10 to 25 | >50 |
| >25 to 50 | >25 |
| >50 | All Projects |

The proposed project disturbs 3.3 acres and is 0.799 acres of impervious. This is approximately 24% impervious cover. A downstream analysis is not required.

3.5.6 Overbank Flood Protection Conclusion

The tables below presents a summary of the pre development flows vs. the mitigated post development flows. The table shows a decrease in the rate of runoff for all storms included in the analysis.

Pre Development Flows vs. Post Development Flows Mitigated

Pre-development Conditions versus Post Development Conditions Flow Rates for each watershed are summarized below:

| Subwatershed (design point) | 1-yr Peak Flow | | 2-yr Peak Flow | | 10-yr Peak Flow | | 25-yr Peak Flow | | 100-yr Peak Flow | |
|--------------------------------|-------------------|------|-------------------|------|--------------------|------|--------------------|------|---------------------|-------|
| | Pre | Post | Pre | Post | Pre | Post | Pre | Post | Pre | Post |
| DP-1: Saugatucket Road | 0.07 | 0.09 | 0.11 | 0.13 | 0.23 | 0.25 | 0.34 | 0.35 | 0.55 | 0.54 |
| DP-2: Wetland A | 1.67 | 1.47 | 2.67 | 2.10 | 6.52 | 4.88 | 9.80 | 8.90 | 16.87 | 16.52 |
| Totals: | 1.74 | 1.56 | 2.78 | 2.23 | 6.75 | 5.13 | 10.14 | 9.25 | 17.42 | 17.06 |

All flows in cubic feet per second (cfs)

As shown in the tables above, minimal to no increase in stormwater runoff flow will occur following the proposed construction during the 1 through 100-year storm events.

3.6 Minimum Standard 6: Redevelopment and Infill Projects.

The site is not classified as a redevelopment or infill project.

3.7 Minimum Standard 7: Pollution Prevention

A Soil Erosion and Sediment Control Plan (SESC) for this development can be found under a separate document. See the Soil Erosion and Sediment Control Plan for the development prepared by DiPrete Engineering. The SESC contains information for construction pollution prevention. For post construction pollution prevention see the Operations and Maintenance (O&M) document prepared for this development by DiPrete Engineering.

3.8 Minimum Standard 8: Land Uses with High Potential Pollutant Loads (LUHPPLs)

The site is not considered LUHPPL.

3.9 Minimum Standard 9: Illicit Discharges

There are no proposed Illicit Discharges on site. The site will be serviced by public water and private OWTS.

3.10 Minimum Standard 10: Construction Activity Soil Erosion, Runoff and Sedimentation and Pollution Prevention Control Measure Requirements

See the SESC for this development prepared by DiPrete Engineering.

3.11 Minimum Standard 11: Stormwater Management System Operation and Maintenance

See the O&M for this development prepared by DiPrete Engineering.

Appendix A

A2.1 Soil Evaluations



STATE OF RHODE ISLAND AND PROVIDENCE PLANTATIONS

Department of Environmental Management
Office of Water Resources
Onsite Wastewater Treatment Systems Program



Site Evaluation Form
Part A - Soil Profile Description

Application Number 2232-1533

Property Owner: Joseph and Donna Randle

Property Location: 176 Saugatucket Road South Kingstown

Date of Test Hole: 12/15/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Overcast, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Rows include Ap, Bw, Cg, 2Cd and several empty rows.

TH D3 Soil Class Loess/dense Total Depth 96" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 96" SHWT 24" (og)

TH Soil Class Total Depth Impervious/Limiting Layer Depth (og) GW Seepage Depth SHWT (og)

Comments:



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Property Location: 176 Saugatucket Road South Kingstown

Date of Test Hole: 12/15/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Sunny, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains two soil profile sections: TH 22-A1 and TH 22A2.

TH 22-A1 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 100" SHWT 21" (og)
TH 22-A2 Soil Class Loess/dense Total Depth 102" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 18" (og)

Comments:



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Date of Test Hole: 12/15/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Sunny, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for two soil profiles: 22-A3 and 22-A4.

TH 22-A3 Soil Class Loess/dense Total Depth 105" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 19" (og)
TH 22-A4 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 18" (og)

Comments:



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Property Location: 176 Saugatucket Road South Kingstown

Date of Test Hole: 12/15/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Overcast, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for two soil profiles: TH 22-A5 and TH 22-A6.

TH 22-A5 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 18" (og)

TH 22-A6 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 21" (og)

Comments: 22-A5 - Ap contains shells, plastic, and wire artifacts.



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Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Overcast, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains two sections for TH 22-A7 and TH 22-A8.

TH 22-A7 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 18" (og)
TH 22-A8 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 18" (og)

Comments:



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Date of Test Hole: 12/16/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Rain, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for two soil profiles: TH 22-A9 and TH A10.

TH 22-A9 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 60" SHWT 18" (og)
TH 22A10 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 60" SHWT 23" (og)

Comments:



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Date of Test Hole: 12/16/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Rain, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. It contains two sections of soil profile data, TH A11 and TH A12.

TH 22A11 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 61" SHWT 19" (og)
TH 22A12 Soil Class Loess/dense Total Depth 120" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 60" SHWT 16" (og)

Comments:



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Property Location: 176 Saugatucket Road South Kingstown

Date of Test Hole: 12/16/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Rain, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains two soil profile sections (A13 and A14).

TH 22A13 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 96" SHWT 27" (og)
TH 22A14 Soil Class Loess/dense Total Depth 108" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 108" SHWT 21" (og)

Comments:



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Property Location: 176 Saugatucket Road South Kingstown

Date of Test Hole: 12/15/2022

Soil Evaluator: Tim Twohig

License Number: D-4073

Weather: Overcast, 40

Shaded: Yes [checked] No [] Time: 8:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for two soil profiles (D1 and D2).

TH D1 Soil Class Loess/dense Total Depth 96" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 36" SHWT 24" (og)
TH D2 Soil Class Loess/dense Total Depth 96" Impervious/Limiting Layer Depth - (og) GW Seepage Depth 80" SHWT 20" (og)

Comments:



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Site Evaluation Form
Part A - Soil Profile Description

Application Number 2232-1533

Property Owner: JAE Mills LLC

Property Location: 176 Saugatucket Road (AP 42, Lot 9), South Kingstown

Date of Test Hole: September 5, 2024

Soil Evaluator: Allison Drake

License Number: D-4105

Weather: Clear, 70's

Shaded: Yes [] No [x] Time: 10:00AM

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains two soil profile sections.

TH STH 24-1 Soil Class Dense Till Total Depth 96" Impervious/Limiting Layer Depth N/A (og) GW Seepage Depth N/A SHWT 18" (og)

TH STH 24-2 Soil Class Dense Till Total Depth 96" Impervious/Limiting Layer Depth N/A (og) GW Seepage Depth N/A SHWT 18" (og)

Comments: [Blank lines for notes]



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Date of Test Hole: September 5, 2024

Soil Evaluator: Allison Drake

License Number: D-4105

Weather: Clear, 70's

Shaded: Yes [] No [x] Time: 10:00AM

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains two soil profile sections.

TH STH 24-3 Soil Class Dense Till Total Depth 96" Impervious/Limiting Layer Depth N/A (og) GW Seepage Depth N/A SHWT 18" (og)

TH STH 24-4 Soil Class Dense Till Total Depth 102" Impervious/Limiting Layer Depth N/A (og) GW Seepage Depth 66" SHWT 12" (og)

Comments: [Blank lines for notes]



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Site Evaluation Form
Part A - Soil Profile Description

Application Number

Property Owner:

Property Location: 176 Saugatucket Road, Wakefield

Date of Test Hole: 11/16/2022

Soil Evaluator: Tim Twohig License Number: D-4073

Weather: 50s, rain Shaded: Yes [checked] No [] Time: 8:00 - 4:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains two sections of soil profile data.

TH 1 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 21" (og)
TH 2 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth - (og) GW Seepage Depth - SHWT 22" (og)

Comments:



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Site Evaluation Form
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Property Owner:

Property Location: 176 Saugatucket Road, Wakefield

Date of Test Hole: 11/16/2022

Soil Evaluator: Tim Twohig License Number: D-4073

Weather: 50s, rain Shaded: Yes [checked] No [] Time: 8:00 - 4:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for two soil profiles (TH 3 and TH 4).

TH 3 Soil Class Loess/Dense Total Depth 94" Impervious/Limiting Layer Depth 46" (og) GW Seepage Depth - SHWT 21" (og)
TH 4 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 61" (og) GW Seepage Depth - SHWT 17" (og)

Comments:



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Application Number

Property Owner:

Property Location: 176 Saugatucket Road, Wakefield

Date of Test Hole: 11/16/2022

Soil Evaluator: Tim Twohig License Number: D-4073

Weather: 50s, rain Shaded: Yes [checked] No [] Time: 8:00 - 4:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Rows include horizons A, Bw, C, 2Cd, Ap, Bw, 2C, 3Cd, R.

TH 5 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 65" (og) GW Seepage Depth - SHWT 13" (og)
TH 6 Soil Class Loess/Dense Total Depth 72" Impervious/Limiting Layer Depth 45" (og) GW Seepage Depth - SHWT 15" (og)

Comments:



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Site Evaluation Form
Part A - Soil Profile Description

Application Number _____

Property Owner: _____

Property Location: 176 Saugatucket Road, Wakefield

Date of Test Hole: 11/16/2022

Soil Evaluator: Tim Twohig License Number: D-4073

Weather: 50s, rain Shaded: Yes [checked] No [] Time: 8:00 - 4:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for TH 7 and TH 8 horizons.

TH 7 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 35" (og) GW Seepage Depth 29" SHWT 9" (og)

TH 8 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 38" (og) GW Seepage Depth 72" SHWT 16" (og)

Comments: _____



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Part A - Soil Profile Description

Application Number _____

Property Owner: _____

Property Location: 176 Saugatucket Road, Wakefield

Date of Test Hole: 11/16/2022

Soil Evaluator: Tim Twohig License Number: D-4073

Weather: 50s, rain Shaded: Yes [checked] No [] Time: 8:00 - 4:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for TH 9 and TH 10 horizons.

TH 9 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 60" (og) GW Seepage Depth - SHWT 11" (og)

TH 10 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 41" (og) GW Seepage Depth 45" SHWT 9" (og)

Comments: _____



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Application Number

Property Owner:

Property Location: 176 Saugatucket Road, Wakefield

Date of Test Hole: 11/16/2022

Soil Evaluator: Tim Twohig License Number: D-4073

Weather: 50s, rain Shaded: Yes [checked] No [] Time: 8:00 - 4:00

Table with 11 columns: TH Horizon, Depth, Horizon Boundaries (Dist, Topo), Soil Colors (Matrix, Re-Dox Features), Re-Dox (Ab., S., Contr.), Texture, Structure, Consistence, Soil Category. Contains data for two soil profiles (TH 11 and TH 12).

TH 11 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 60" (og) GW Seepage Depth - SHWT 18" (og)
TH 12 Soil Class Loess/Dense Total Depth 120" Impervious/Limiting Layer Depth 70" (og) GW Seepage Depth 60" SHWT 16" (og)

Comments:

| Date | Site | soil type | horizon | depth to hole bottom* | # chambers | area chambers (cm ²) | depth water in hole (cm) | cm ³ /hour | | | | | | | | |
|----------|----------|----------------|----------|--------------------------|------------|-------------------------------------|-----------------------------|-----------------------|-----------|---------|----------|----------|------|--------------|--------------|-------------|
| | | | | | | | | drop (cm) | drop (in) | minutes | hour | coeff A | Q | Ksat (cm/hr) | Ksat (in/hr) | Ksat (µm/s) |
| 20240923 | AMT 24-1 | FSL/Dense Till | Bw (FSL) | 24" | 2 | 105 | 14 | 0.38 | 0.15 | 0.5 | 0.008333 | 0.001288 | 4788 | 6.166944 | 2.42793202 | 17.1304137 |
| 20240923 | AMT 24-2 | FSL/Dense Till | Bw (FSL) | 21" | 2 | 105 | 14 | 0.31 | 0.12 | 0.5 | 0.008333 | 0.001288 | 3906 | 5.030928 | 1.98068138 | 13.9748112 |
| 20240923 | AMT 24-3 | FSL/Dense Till | Bw (FSL) | 21" | 2 | 105 | 14 | 0.33 | 0.13 | 0.5 | 0.008333 | 0.001288 | 4158 | 5.355504 | 2.10846728 | 14.8764119 |
| 20240923 | AMT 24-4 | FSL/Dense Till | Bw (FSL) | 20" | 2 | 105 | 14 | 0.4 | 0.16 | 0.5 | 0.008333 | 0.001288 | 5040 | 6.49152 | 2.55571792 | 18.0320144 |
| 20240923 | AMT 24-5 | FSL/Dense Till | Bw (FSL) | 20" | 2 | 105 | 14 | 0.31 | 0.12 | 0.5 | 0.008333 | 0.001288 | 3906 | 5.030928 | 1.98068138 | 13.9748112 |

A3.2 Water Quality HydroCAD Storm Analysis

3287-001-ALLS-EHCD-INHS

Type III 24-hr WQ Storm Rainfall=1.20"

Prepared by DiPrete Engineering

Printed 10/10/2024

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv.
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11: WPre-01 Runoff Area=0.088 ac 13.69% Impervious Runoff Depth=0.16"
Tc=6.0 min CN=71/98 Runoff=0.01 cfs 0.001 af

Link 12: DP-1: Saugatcket Road - West Inflow=0.01 cfs 0.001 af
Primary=0.01 cfs 0.001 af

Subcatchment 21: WPre-02 Runoff Area=1.378 ac 3.47% Impervious Runoff Depth=0.05"
Flow Length=437' Tc=16.3 min CN=69/98 Runoff=0.04 cfs 0.006 af

Subcatchment 22: WPre-03 Runoff Area=1.815 ac 4.37% Impervious Runoff Depth=0.05"
Flow Length=454' Tc=8.8 min CN=66/98 Runoff=0.08 cfs 0.007 af

Subcatchment 23: WPre-04 Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=0.00"
Flow Length=245' Tc=13.2 min CN=65/0 Runoff=0.00 cfs 0.000 af

Subcatchment 24: WPre-05 Runoff Area=0.318 ac 55.92% Impervious Runoff Depth=0.58"
Tc=6.0 min CN=74/98 Runoff=0.19 cfs 0.015 af

Link 25: DP-2: Wetland A Inflow=0.30 cfs 0.029 af
Primary=0.30 cfs 0.029 af

3287-001-ALLS-PHCD-INHS

Type III 24-hr WQ Storm Rainfall=1.20"

Prepared by DiPrete Engineering

Printed 1/17/2025

HydroCAD® 10.20-5c s/n 01125 © 2023 HydroCAD Software Solutions LLC

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
 Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv.
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Pond 1P: Lot 1 WQ Drywell Peak Elev=101.96' Storage=0.001 af Inflow=0.05 cfs 0.004 af
 Discarded=0.01 cfs 0.004 af Primary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.004 af

Pond 2P: Lot 2 WQ Drywell Peak Elev=94.96' Storage=0.001 af Inflow=0.05 cfs 0.004 af
 Discarded=0.01 cfs 0.004 af Primary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.004 af

Pond 3P: Lot 3 WQ Drywell Peak Elev=94.71' Storage=0.001 af Inflow=0.05 cfs 0.004 af
 Discarded=0.01 cfs 0.004 af Primary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.004 af

Pond 4P: Lot 4 WQ Drywell Peak Elev=96.66' Storage=0.001 af Inflow=0.05 cfs 0.004 af
 Discarded=0.01 cfs 0.004 af Primary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.004 af

Pond 5P: Lot 5 WQ Drywell Peak Elev=98.42' Storage=0.001 af Inflow=0.05 cfs 0.004 af
 Discarded=0.01 cfs 0.004 af Primary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.004 af

Subcatchment 101: WPost-01 Runoff Area=0.079 ac 19.72% Impervious Runoff Depth=0.24"
 Tc=6.0 min CN=74/98 Runoff=0.02 cfs 0.002 af

Link 102: DP-1: Saugatucket Road - West Inflow=0.02 cfs 0.002 af
 Primary=0.02 cfs 0.002 af

Subcatchment 201: WPost-02 Runoff Area=1.479 ac 3.22% Impervious Runoff Depth=0.07"
 Flow Length=239' Tc=10.9 min CN=72/98 Runoff=0.04 cfs 0.009 af

Subcatchment 202: WPost-03 Runoff Area=0.361 ac 50.91% Impervious Runoff Depth=0.53"
 Tc=6.0 min CN=73/98 Runoff=0.20 cfs 0.016 af

Subcatchment 203: WPost-04 Runoff Area=1.821 ac 27.95% Impervious Runoff Depth=0.32"
 Flow Length=165' Tc=15.8 min CN=74/98 Runoff=0.42 cfs 0.049 af

Pond 204: Forebay A Peak Elev=95.58' Storage=667 cf Inflow=0.42 cfs 0.049 af
 Primary=0.38 cfs 0.049 af Secondary=0.00 cfs 0.000 af Outflow=0.38 cfs 0.049 af

Subcatchment 205: WPost-05 Runoff Area=0.059 ac 0.00% Impervious Runoff Depth=0.06"
 Tc=0.0 min CN=74/0 Runoff=0.00 cfs 0.000 af

Pond 206: WQ Infiltration Pond A Peak Elev=95.58' Storage=884 cf Inflow=0.39 cfs 0.049 af
 Discarded=0.02 cfs 0.049 af Primary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.049 af

Subcatchment 207: WPost-06 Runoff Area=0.154 ac 0.00% Impervious Runoff Depth=0.06"
 Tc=0.0 min CN=74/0 Runoff=0.00 cfs 0.001 af

Pond 208: Infiltration Pond A Peak Elev=94.50' Storage=1 cf Inflow=0.00 cfs 0.001 af
 Discarded=0.00 cfs 0.001 af Primary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.001 af

Link 209: DP-2: Wetland A Inflow=0.24 cfs 0.025 af
 Primary=0.24 cfs 0.025 af

3287-001-ALLS-PHCD-INHS

Prepared by DiPrete Engineering

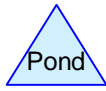
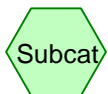
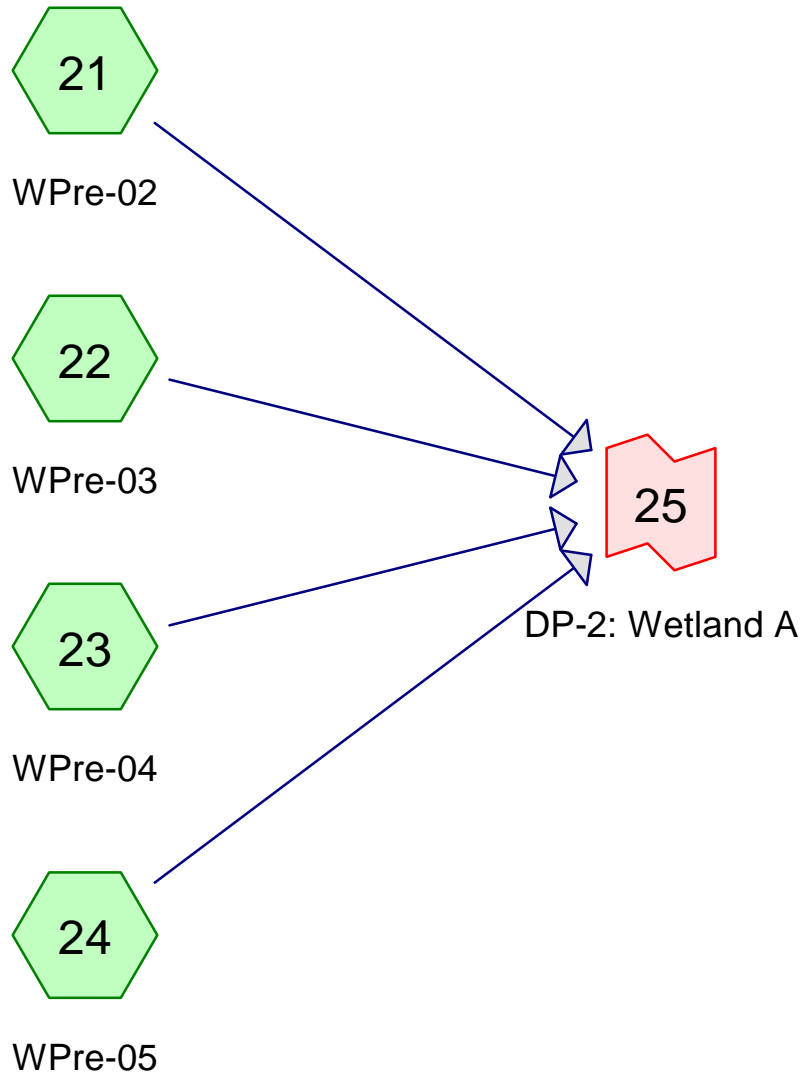
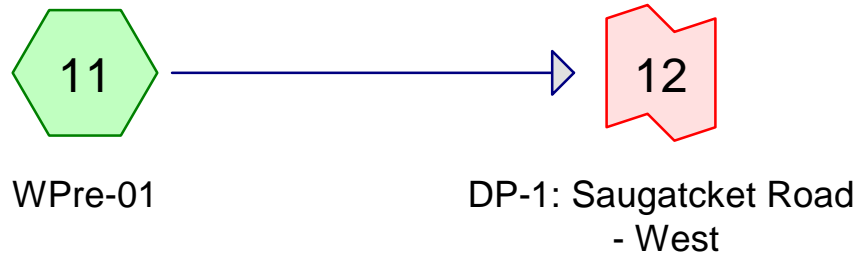
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Type III 24-hr WQ Storm Rainfall=1.20"

Printed 1/17/2025

| | |
|------------------------------------|---|
| Subcatchment L1: Lot 1 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=0.99" Tc=6.0 min CN=0/98 Runoff=0.05 cfs 0.004 af |
| Subcatchment L2: Lot 2 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=0.99" Tc=6.0 min CN=0/98 Runoff=0.05 cfs 0.004 af |
| Subcatchment L3: Lot 3 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=0.99" Tc=6.0 min CN=0/98 Runoff=0.05 cfs 0.004 af |
| Subcatchment L4: Lot 4 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=0.99" Tc=6.0 min CN=0/98 Runoff=0.05 cfs 0.004 af |
| Subcatchment L5: Lot 5 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=0.99" Tc=6.0 min CN=0/98 Runoff=0.05 cfs 0.004 af |

A3.4.2 HydroCAD Node Diagram



Routing Diagram for 3287-001-ALLS-EHCD-INHS
 Prepared by DiPrete Engineering, Printed 10/10/2024
 HydroCAD® 10.20-3g s/n 01125 © 2023 HydroCAD Software Solutions LLC

3287-001-ALLS-EHCD-INHS

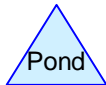
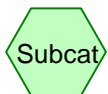
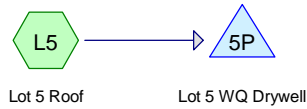
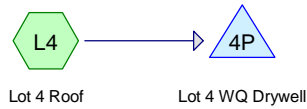
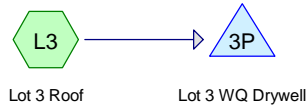
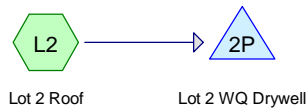
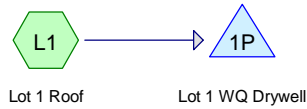
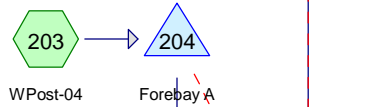
Prepared by DiPrete Engineering

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Printed 10/10/2024

Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|-----------|--|
| 0.840 | 74 | >75% Grass cover, Good, HSG C (11, 21, 22, 23, 24) |
| 2.560 | 65 | Brush, Good, HSG C (11, 21, 22, 23, 24) |
| 0.074 | 98 | Impervious, HSG C (21, 22, 24) |
| 0.189 | 98 | Offsite Impervious, HSG C (11, 24) |
| 0.054 | 98 | Roofs, HSG C (21, 22) |
| 0.226 | 70 | Woods, Good, HSG C (11, 21, 22, 24) |
| 3.943 | 70 | TOTAL AREA |



Routing Diagram for 3287-001-ALLS-PHCD-INHS
 Prepared by DiPrete Engineering, Printed 1/17/2025
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3287-001-ALLS-PHCD-INHS

Prepared by DiPrete Engineering

Printed 1/17/2025

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Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|-----------|--|
| 2.819 | 74 | >75% Grass cover, Good, HSG C (101, 201, 202, 203, 205, 207) |
| 0.307 | 65 | Brush, Good, HSG C (201, 202) |
| 0.322 | 98 | Impervious, HSG C (101, 202, 203) |
| 0.196 | 98 | Offsite Impervious, HSG C (101, 202) |
| 0.477 | 98 | Roofs, HSG C (201, 203, L1, L2, L3, L4, L5) |
| 0.070 | 70 | Woods, Good, HSG C (201) |
| 4.190 | 79 | TOTAL AREA |

A3.5.4.1 HydroCAD 1-Year Storm Analysis

3287-001-ALLS-EHCD-INHS

Prepared by DiPrete Engineering

HydroCAD® 10.20-3g s/n 01125 © 2023 HydroCAD Software Solutions LLC

Type III 24-hr 1-Year Rainfall=2.80"

Printed 10/10/2024

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11: WPre-01 Runoff Area=0.088 ac 13.69% Impervious Runoff Depth=0.78"
Tc=6.0 min CN=74 Runoff=0.07 cfs 0.006 af

Link 12: DP-1: Saugatcket Road - West Inflow=0.07 cfs 0.006 af
Primary=0.07 cfs 0.006 af

Subcatchment 21: WPre-02 Runoff Area=1.378 ac 3.47% Impervious Runoff Depth=0.61"
Flow Length=437' Tc=16.3 min CN=70 Runoff=0.59 cfs 0.070 af

Subcatchment 22: WPre-03 Runoff Area=1.815 ac 4.37% Impervious Runoff Depth=0.49"
Flow Length=454' Tc=8.8 min CN=67 Runoff=0.70 cfs 0.074 af

Subcatchment 23: WPre-04 Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=0.42"
Flow Length=245' Tc=13.2 min CN=65 Runoff=0.09 cfs 0.012 af

Subcatchment 24: WPre-05 Runoff Area=0.318 ac 55.92% Impervious Runoff Depth=1.57"
Tc=6.0 min CN=87 Runoff=0.58 cfs 0.041 af

Link 25: DP-2: Wetland A Inflow=1.67 cfs 0.197 af
Primary=1.67 cfs 0.197 af

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Pond 1P: Lot 1 WQ Drywell Peak Elev=103.11' Storage=0.001 af Inflow=0.13 cfs 0.010 af
 Discarded=0.01 cfs 0.007 af Primary=0.12 cfs 0.003 af Outflow=0.13 cfs 0.010 af

Pond 2P: Lot 2 WQ Drywell Peak Elev=96.06' Storage=0.003 af Inflow=0.13 cfs 0.010 af
 Discarded=0.01 cfs 0.007 af Primary=0.05 cfs 0.003 af Outflow=0.06 cfs 0.010 af

Pond 3P: Lot 3 WQ Drywell Peak Elev=96.86' Storage=0.001 af Inflow=0.13 cfs 0.010 af
 Discarded=0.01 cfs 0.007 af Primary=0.12 cfs 0.003 af Outflow=0.13 cfs 0.010 af

Pond 4P: Lot 4 WQ Drywell Peak Elev=97.86' Storage=0.001 af Inflow=0.13 cfs 0.010 af
 Discarded=0.01 cfs 0.008 af Primary=0.12 cfs 0.003 af Outflow=0.13 cfs 0.010 af

Pond 5P: Lot 5 WQ Drywell Peak Elev=99.61' Storage=0.001 af Inflow=0.13 cfs 0.010 af
 Discarded=0.01 cfs 0.007 af Primary=0.12 cfs 0.003 af Outflow=0.13 cfs 0.010 af

Subcatchment 101: WPost-01 Runoff Area=0.079 ac 19.72% Impervious Runoff Depth=1.04"
 Tc=6.0 min CN=79 Runoff=0.09 cfs 0.007 af

Link 102: DP-1: Saugatucket Road - West Inflow=0.09 cfs 0.007 af
 Primary=0.09 cfs 0.007 af

Subcatchment 201: WPost-02 Runoff Area=1.479 ac 3.22% Impervious Runoff Depth=0.74"
 Flow Length=239' Tc=10.9 min CN=73 Runoff=0.97 cfs 0.091 af

Subcatchment 202: WPost-03 Runoff Area=0.361 ac 50.91% Impervious Runoff Depth=1.49"
 Tc=6.0 min CN=86 Runoff=0.63 cfs 0.045 af

Subcatchment 203: WPost-04 Runoff Area=1.821 ac 27.95% Impervious Runoff Depth=1.16"
 Flow Length=165' Tc=15.8 min CN=81 Runoff=1.80 cfs 0.176 af

Pond 204: Forebay A Peak Elev=95.80' Storage=845 cf Inflow=1.80 cfs 0.176 af
 Primary=0.80 cfs 0.052 af Secondary=1.61 cfs 0.124 af Outflow=1.67 cfs 0.176 af

Subcatchment 205: WPost-05 Runoff Area=0.059 ac 0.00% Impervious Runoff Depth=0.78"
 Tc=0.0 min CN=74 Runoff=0.06 cfs 0.004 af

Pond 206: WQ Infiltration Pond A Peak Elev=95.80' Storage=1,113 cf Inflow=0.83 cfs 0.056 af
 Discarded=0.02 cfs 0.056 af Primary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.056 af

Subcatchment 207: WPost-06 Runoff Area=0.154 ac 0.00% Impervious Runoff Depth=0.78"
 Tc=0.0 min CN=74 Runoff=0.16 cfs 0.010 af

Pond 208: Infiltration Pond A Peak Elev=95.63' Storage=3,581 cf Inflow=1.66 cfs 0.134 af
 Discarded=0.08 cfs 0.134 af Primary=0.00 cfs 0.000 af Outflow=0.08 cfs 0.134 af

Link 209: DP-2: Wetland A Inflow=1.47 cfs 0.136 af
 Primary=1.47 cfs 0.136 af

3287-001-ALLS-PHCD-INHS

Prepared by DiPrete Engineering

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Type III 24-hr 1-Year Rainfall=2.80"

Printed 1/17/2025

| | |
|------------------------------------|---|
| Subcatchment L1: Lot 1 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=2.57" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af |
| Subcatchment L2: Lot 2 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=2.57" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af |
| Subcatchment L3: Lot 3 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=2.57" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af |
| Subcatchment L4: Lot 4 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=2.57" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af |
| Subcatchment L5: Lot 5 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=2.57" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af |

A3.5.4.2 HydroCAD 2-Year Storm Analysis

3287-001-ALLS-EHCD-INHS

Prepared by DiPrete Engineering

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Type III 24-hr 2-Year Rainfall=3.30"

Printed 10/10/2024

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11: WPre-01 Runoff Area=0.088 ac 13.69% Impervious Runoff Depth=1.10"
Tc=6.0 min CN=74 Runoff=0.11 cfs 0.008 af

Link 12: DP-1: Saugatcket Road - West Inflow=0.11 cfs 0.008 af
Primary=0.11 cfs 0.008 af

Subcatchment 21: WPre-02 Runoff Area=1.378 ac 3.47% Impervious Runoff Depth=0.89"
Flow Length=437' Tc=16.3 min CN=70 Runoff=0.94 cfs 0.102 af

Subcatchment 22: WPre-03 Runoff Area=1.815 ac 4.37% Impervious Runoff Depth=0.74"
Flow Length=454' Tc=8.8 min CN=67 Runoff=1.21 cfs 0.112 af

Subcatchment 23: WPre-04 Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=0.65"
Flow Length=245' Tc=13.2 min CN=65 Runoff=0.16 cfs 0.019 af

Subcatchment 24: WPre-05 Runoff Area=0.318 ac 55.92% Impervious Runoff Depth=2.00"
Tc=6.0 min CN=87 Runoff=0.75 cfs 0.053 af

Link 25: DP-2: Wetland A Inflow=2.67 cfs 0.286 af
Primary=2.67 cfs 0.286 af

3287-001-ALLS-PHCD-INHS

Type III 24-hr 2-Year Rainfall=3.30"

Prepared by DiPrete Engineering

Printed 1/17/2025

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Pond 1P: Lot 1 WQ Drywell Peak Elev=103.12' Storage=0.001 af Inflow=0.15 cfs 0.012 af
 Discarded=0.01 cfs 0.008 af Primary=0.14 cfs 0.004 af Outflow=0.15 cfs 0.012 af

Pond 2P: Lot 2 WQ Drywell Peak Elev=96.08' Storage=0.003 af Inflow=0.15 cfs 0.012 af
 Discarded=0.01 cfs 0.008 af Primary=0.08 cfs 0.004 af Outflow=0.08 cfs 0.012 af

Pond 3P: Lot 3 WQ Drywell Peak Elev=96.87' Storage=0.001 af Inflow=0.15 cfs 0.012 af
 Discarded=0.01 cfs 0.008 af Primary=0.14 cfs 0.004 af Outflow=0.15 cfs 0.012 af

Pond 4P: Lot 4 WQ Drywell Peak Elev=97.87' Storage=0.001 af Inflow=0.15 cfs 0.012 af
 Discarded=0.01 cfs 0.008 af Primary=0.14 cfs 0.004 af Outflow=0.15 cfs 0.012 af

Pond 5P: Lot 5 WQ Drywell Peak Elev=99.62' Storage=0.001 af Inflow=0.15 cfs 0.012 af
 Discarded=0.01 cfs 0.008 af Primary=0.14 cfs 0.004 af Outflow=0.15 cfs 0.012 af

Subcatchment 101: WPost-01 Runoff Area=0.079 ac 19.72% Impervious Runoff Depth=1.41"
 Tc=6.0 min CN=79 Runoff=0.13 cfs 0.009 af

Link 102: DP-1: Saugatucket Road - West Inflow=0.13 cfs 0.009 af
 Primary=0.13 cfs 0.009 af

Subcatchment 201: WPost-02 Runoff Area=1.479 ac 3.22% Impervious Runoff Depth=1.05"
 Flow Length=239' Tc=10.9 min CN=73 Runoff=1.45 cfs 0.129 af

Subcatchment 202: WPost-03 Runoff Area=0.361 ac 50.91% Impervious Runoff Depth=1.92"
 Tc=6.0 min CN=86 Runoff=0.81 cfs 0.058 af

Subcatchment 203: WPost-04 Runoff Area=1.821 ac 27.95% Impervious Runoff Depth=1.55"
 Flow Length=165' Tc=15.8 min CN=81 Runoff=2.43 cfs 0.235 af

Pond 204: Forebay A Peak Elev=95.84' Storage=886 cf Inflow=2.43 cfs 0.235 af
 Primary=0.60 cfs 0.052 af Secondary=2.38 cfs 0.182 af Outflow=2.38 cfs 0.235 af

Subcatchment 205: WPost-05 Runoff Area=0.059 ac 0.00% Impervious Runoff Depth=1.10"
 Tc=0.0 min CN=74 Runoff=0.09 cfs 0.005 af

Pond 206: WQ Infiltration Pond A Peak Elev=95.84' Storage=1,163 cf Inflow=0.67 cfs 0.058 af
 Discarded=0.03 cfs 0.058 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.058 af

Subcatchment 207: WPost-06 Runoff Area=0.154 ac 0.00% Impervious Runoff Depth=1.10"
 Tc=0.0 min CN=74 Runoff=0.23 cfs 0.014 af

Pond 208: Infiltration Pond A Peak Elev=95.81' Storage=4,248 cf Inflow=2.46 cfs 0.197 af
 Discarded=0.09 cfs 0.160 af Primary=0.20 cfs 0.037 af Outflow=0.29 cfs 0.197 af

Link 209: DP-2: Wetland A Inflow=2.10 cfs 0.224 af
 Primary=2.10 cfs 0.224 af

3287-001-ALLS-PHCD-INHS

Prepared by DiPrete Engineering

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Type III 24-hr 2-Year Rainfall=3.30"

Printed 1/17/2025

| | |
|------------------------------------|---|
| Subcatchment L1: Lot 1 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af |
| Subcatchment L2: Lot 2 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af |
| Subcatchment L3: Lot 3 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af |
| Subcatchment L4: Lot 4 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af |
| Subcatchment L5: Lot 5 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af |

A3.5.4.3 HydroCAD 10-Year Storm Analysis

3287-001-ALLS-EHCD-INHS

Prepared by DiPrete Engineering

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Type III 24-hr 10-Year Rainfall=4.90"

Printed 10/10/2024

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11: WPre-01 Runoff Area=0.088 ac 13.69% Impervious Runoff Depth=2.28"
Tc=6.0 min CN=74 Runoff=0.23 cfs 0.017 af

Link 12: DP-1: Saugatcket Road - West Inflow=0.23 cfs 0.017 af
Primary=0.23 cfs 0.017 af

Subcatchment 21: WPre-02 Runoff Area=1.378 ac 3.47% Impervious Runoff Depth=1.96"
Flow Length=437' Tc=16.3 min CN=70 Runoff=2.27 cfs 0.225 af

Subcatchment 22: WPre-03 Runoff Area=1.815 ac 4.37% Impervious Runoff Depth=1.73"
Flow Length=454' Tc=8.8 min CN=67 Runoff=3.22 cfs 0.262 af

Subcatchment 23: WPre-04 Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=1.59"
Flow Length=245' Tc=13.2 min CN=65 Runoff=0.48 cfs 0.045 af

Subcatchment 24: WPre-05 Runoff Area=0.318 ac 55.92% Impervious Runoff Depth=3.47"
Tc=6.0 min CN=87 Runoff=1.27 cfs 0.092 af

Link 25: DP-2: Wetland A Inflow=6.52 cfs 0.625 af
Primary=6.52 cfs 0.625 af

3287-001-ALLS-PHCD-INHS

Type III 24-hr 10-Year Rainfall=4.90"

Prepared by DiPrete Engineering

Printed 1/17/2025

HydroCAD® 10.20-5c s/n 01125 © 2023 HydroCAD Software Solutions LLC

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Pond 1P: Lot 1 WQ Drywell Peak Elev=103.23' Storage=0.002 af Inflow=0.23 cfs 0.019 af
 Discarded=0.01 cfs 0.010 af Primary=0.20 cfs 0.009 af Outflow=0.21 cfs 0.019 af

Pond 2P: Lot 2 WQ Drywell Peak Elev=96.12' Storage=0.004 af Inflow=0.23 cfs 0.019 af
 Discarded=0.01 cfs 0.010 af Primary=0.15 cfs 0.009 af Outflow=0.15 cfs 0.019 af

Pond 3P: Lot 3 WQ Drywell Peak Elev=96.99' Storage=0.002 af Inflow=0.23 cfs 0.019 af
 Discarded=0.01 cfs 0.010 af Primary=0.20 cfs 0.009 af Outflow=0.21 cfs 0.019 af

Pond 4P: Lot 4 WQ Drywell Peak Elev=97.99' Storage=0.002 af Inflow=0.23 cfs 0.019 af
 Discarded=0.01 cfs 0.011 af Primary=0.20 cfs 0.008 af Outflow=0.21 cfs 0.019 af

Pond 5P: Lot 5 WQ Drywell Peak Elev=99.73' Storage=0.002 af Inflow=0.23 cfs 0.019 af
 Discarded=0.01 cfs 0.011 af Primary=0.20 cfs 0.008 af Outflow=0.21 cfs 0.019 af

Subcatchment 101: WPost-01 Runoff Area=0.079 ac 19.72% Impervious Runoff Depth=2.72"
 Tc=6.0 min CN=79 Runoff=0.25 cfs 0.018 af

Link 102: DP-1: Saugatucket Road - West Inflow=0.25 cfs 0.018 af
 Primary=0.25 cfs 0.018 af

Subcatchment 201: WPost-02 Runoff Area=1.479 ac 3.22% Impervious Runoff Depth=2.20"
 Flow Length=239' Tc=10.9 min CN=73 Runoff=3.21 cfs 0.271 af

Subcatchment 202: WPost-03 Runoff Area=0.361 ac 50.91% Impervious Runoff Depth=3.37"
 Tc=6.0 min CN=86 Runoff=1.41 cfs 0.101 af

Subcatchment 203: WPost-04 Runoff Area=1.821 ac 27.95% Impervious Runoff Depth=2.90"
 Flow Length=165' Tc=15.8 min CN=81 Runoff=4.58 cfs 0.440 af

Pond 204: Forebay A Peak Elev=96.10' Storage=1,168 cf Inflow=4.58 cfs 0.440 af
 Primary=0.33 cfs 0.052 af Secondary=4.38 cfs 0.388 af Outflow=4.46 cfs 0.440 af

Subcatchment 205: WPost-05 Runoff Area=0.059 ac 0.00% Impervious Runoff Depth=2.28"
 Tc=0.0 min CN=74 Runoff=0.19 cfs 0.011 af

Pond 206: WQ Infiltration Pond A Peak Elev=96.10' Storage=1,457 cf Inflow=0.39 cfs 0.063 af
 Discarded=0.03 cfs 0.063 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.063 af

Subcatchment 207: WPost-06 Runoff Area=0.154 ac 0.00% Impervious Runoff Depth=2.28"
 Tc=0.0 min CN=74 Runoff=0.50 cfs 0.029 af

Pond 208: Infiltration Pond A Peak Elev=96.09' Storage=5,303 cf Inflow=4.57 cfs 0.417 af
 Discarded=0.09 cfs 0.180 af Primary=2.80 cfs 0.236 af Outflow=2.89 cfs 0.417 af

Link 209: DP-2: Wetland A Inflow=4.88 cfs 0.609 af
 Primary=4.88 cfs 0.609 af

3287-001-ALLS-PHCD-INHS

Prepared by DiPrete Engineering

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Type III 24-hr 10-Year Rainfall=4.90"

Printed 1/17/2025

| | |
|------------------------------------|---|
| Subcatchment L1: Lot 1 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=4.66" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af |
| Subcatchment L2: Lot 2 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=4.66" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af |
| Subcatchment L3: Lot 3 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=4.66" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af |
| Subcatchment L4: Lot 4 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=4.66" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af |
| Subcatchment L5: Lot 5 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=4.66" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af |

A3.5.4.4 HydroCAD 25-Year Storm Analysis

3287-001-ALLS-EHCD-INHS

Prepared by DiPrete Engineering
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Type III 24-hr 25-Year Rainfall=6.10"

Printed 10/10/2024

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11: WPre-01

Runoff Area=0.088 ac 13.69% Impervious Runoff Depth=3.27"
Tc=6.0 min CN=74 Runoff=0.34 cfs 0.024 af

Link 12: DP-1: Saugatcket Road - West

Inflow=0.34 cfs 0.024 af
Primary=0.34 cfs 0.024 af

Subcatchment 21: WPre-02

Runoff Area=1.378 ac 3.47% Impervious Runoff Depth=2.88"
Flow Length=437' Tc=16.3 min CN=70 Runoff=3.39 cfs 0.331 af

Subcatchment 22: WPre-03

Runoff Area=1.815 ac 4.37% Impervious Runoff Depth=2.61"
Flow Length=454' Tc=8.8 min CN=67 Runoff=4.96 cfs 0.394 af

Subcatchment 23: WPre-04

Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=2.42"
Flow Length=245' Tc=13.2 min CN=65 Runoff=0.76 cfs 0.069 af

Subcatchment 24: WPre-05

Runoff Area=0.318 ac 55.92% Impervious Runoff Depth=4.61"
Tc=6.0 min CN=87 Runoff=1.67 cfs 0.122 af

Link 25: DP-2: Wetland A

Inflow=9.80 cfs 0.917 af
Primary=9.80 cfs 0.917 af

3287-001-ALLS-PHCD-INHS

Type III 24-hr 25-Year Rainfall=6.10"

Prepared by DiPrete Engineering

Printed 1/17/2025

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Pond 1P: Lot 1 WQ Drywell Peak Elev=103.34' Storage=0.002 af Inflow=0.28 cfs 0.023 af
 Discarded=0.01 cfs 0.011 af Primary=0.25 cfs 0.012 af Outflow=0.25 cfs 0.023 af

Pond 2P: Lot 2 WQ Drywell Peak Elev=96.16' Storage=0.004 af Inflow=0.28 cfs 0.023 af
 Discarded=0.01 cfs 0.011 af Primary=0.17 cfs 0.012 af Outflow=0.17 cfs 0.023 af

Pond 3P: Lot 3 WQ Drywell Peak Elev=97.10' Storage=0.002 af Inflow=0.28 cfs 0.023 af
 Discarded=0.01 cfs 0.011 af Primary=0.25 cfs 0.012 af Outflow=0.26 cfs 0.023 af

Pond 4P: Lot 4 WQ Drywell Peak Elev=98.11' Storage=0.002 af Inflow=0.28 cfs 0.023 af
 Discarded=0.01 cfs 0.012 af Primary=0.25 cfs 0.011 af Outflow=0.26 cfs 0.023 af

Pond 5P: Lot 5 WQ Drywell Peak Elev=99.84' Storage=0.002 af Inflow=0.28 cfs 0.023 af
 Discarded=0.01 cfs 0.012 af Primary=0.25 cfs 0.011 af Outflow=0.25 cfs 0.023 af

Subcatchment 101: WPost-01 Runoff Area=0.079 ac 19.72% Impervious Runoff Depth=3.77"
 Tc=6.0 min CN=79 Runoff=0.35 cfs 0.025 af

Link 102: DP-1: Saugatucket Road - West Inflow=0.35 cfs 0.025 af
 Primary=0.35 cfs 0.025 af

Subcatchment 201: WPost-02 Runoff Area=1.479 ac 3.22% Impervious Runoff Depth=3.17"
 Flow Length=239' Tc=10.9 min CN=73 Runoff=4.67 cfs 0.391 af

Subcatchment 202: WPost-03 Runoff Area=0.361 ac 50.91% Impervious Runoff Depth=4.50"
 Tc=6.0 min CN=86 Runoff=1.86 cfs 0.135 af

Subcatchment 203: WPost-04 Runoff Area=1.821 ac 27.95% Impervious Runoff Depth=3.97"
 Flow Length=165' Tc=15.8 min CN=81 Runoff=6.26 cfs 0.603 af

Pond 204: Forebay A Peak Elev=96.26' Storage=1,386 cf Inflow=6.26 cfs 0.603 af
 Primary=0.53 cfs 0.051 af Secondary=5.31 cfs 0.552 af Outflow=5.76 cfs 0.603 af

Subcatchment 205: WPost-05 Runoff Area=0.059 ac 0.00% Impervious Runoff Depth=3.27"
 Tc=0.0 min CN=74 Runoff=0.28 cfs 0.016 af

Pond 206: WQ Infiltration Pond A Peak Elev=96.27' Storage=1,670 cf Inflow=0.64 cfs 0.067 af
 Discarded=0.03 cfs 0.067 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.067 af

Subcatchment 207: WPost-06 Runoff Area=0.154 ac 0.00% Impervious Runoff Depth=3.27"
 Tc=0.0 min CN=74 Runoff=0.72 cfs 0.042 af

Pond 208: Infiltration Pond A Peak Elev=96.23' Storage=5,896 cf Inflow=5.55 cfs 0.594 af
 Discarded=0.09 cfs 0.189 af Primary=5.04 cfs 0.405 af Outflow=5.13 cfs 0.594 af

Link 209: DP-2: Wetland A Inflow=8.90 cfs 0.932 af
 Primary=8.90 cfs 0.932 af

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Prepared by DiPrete Engineering

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Type III 24-hr 25-Year Rainfall=6.10"

Printed 1/17/2025

| | |
|------------------------------------|---|
| Subcatchment L1: Lot 1 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=5.86" Tc=6.0 min CN=98 Runoff=0.28 cfs 0.023 af |
| Subcatchment L2: Lot 2 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=5.86" Tc=6.0 min CN=98 Runoff=0.28 cfs 0.023 af |
| Subcatchment L3: Lot 3 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=5.86" Tc=6.0 min CN=98 Runoff=0.28 cfs 0.023 af |
| Subcatchment L4: Lot 4 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=5.86" Tc=6.0 min CN=98 Runoff=0.28 cfs 0.023 af |
| Subcatchment L5: Lot 5 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=5.86" Tc=6.0 min CN=98 Runoff=0.28 cfs 0.023 af |

A3.5.4.5 HydroCAD 100-Year Storm Analysis

3287-001-ALLS-EHCD-INHS

Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 10/10/2024

HydroCAD® 10.20-3g s/n 01125 © 2023 HydroCAD Software Solutions LLC

Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 11: WPre-01 Runoff Area=0.088 ac 13.69% Impervious Runoff Depth=5.38"
Tc=6.0 min CN=74 Runoff=0.55 cfs 0.039 af

Link 12: DP-1: Saugatcket Road - West Inflow=0.55 cfs 0.039 af
Primary=0.55 cfs 0.039 af

Subcatchment 21: WPre-02 Runoff Area=1.378 ac 3.47% Impervious Runoff Depth=4.90"
Flow Length=437' Tc=16.3 min CN=70 Runoff=5.80 cfs 0.562 af

Subcatchment 22: WPre-03 Runoff Area=1.815 ac 4.37% Impervious Runoff Depth=4.54"
Flow Length=454' Tc=8.8 min CN=67 Runoff=8.77 cfs 0.687 af

Subcatchment 23: WPre-04 Runoff Area=0.344 ac 0.00% Impervious Runoff Depth=4.30"
Flow Length=245' Tc=13.2 min CN=65 Runoff=1.37 cfs 0.123 af

Subcatchment 24: WPre-05 Runoff Area=0.318 ac 55.92% Impervious Runoff Depth=6.94"
Tc=6.0 min CN=87 Runoff=2.46 cfs 0.184 af

Link 25: DP-2: Wetland A Inflow=16.87 cfs 1.556 af
Primary=16.87 cfs 1.556 af

3287-001-ALLS-EHCD-INHS

Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 10/10/2024

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Summary for Subcatchment 11: WPre-01

Runoff = 0.55 cfs @ 12.09 hrs, Volume= 0.039 af, Depth= 5.38"

Routed to Link 12 : DP-1: Saugatcket Road - West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.038 | 74 | >75% Grass cover, Good, HSG C |
| 0.019 | 65 | Brush, Good, HSG C |
| 0.012 | 98 | Offsite Impervious, HSG C |
| 0.018 | 70 | Woods, Good, HSG C |
| 0.088 | 74 | Weighted Average |
| 0.076 | 71 | 86.31% Pervious Area |
| 0.012 | 98 | 13.69% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---------------|
| 6.0 | | | | | Direct Entry, |

Summary for Link 12: DP-1: Saugatcket Road - West

Inflow Area = 0.088 ac, 13.69% Impervious, Inflow Depth = 5.38" for 100-Year event

Inflow = 0.55 cfs @ 12.09 hrs, Volume= 0.039 af

Primary = 0.55 cfs @ 12.09 hrs, Volume= 0.039 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Subcatchment 21: WPre-02

Runoff = 5.80 cfs @ 12.22 hrs, Volume= 0.562 af, Depth= 4.90"

Routed to Link 25 : DP-2: Wetland A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.460 | 74 | >75% Grass cover, Good, HSG C |
| 0.699 | 65 | Brush, Good, HSG C |
| 0.038 | 98 | Impervious, HSG C |
| 0.009 | 98 | Roofs, HSG C |
| 0.172 | 70 | Woods, Good, HSG C |
| 1.378 | 70 | Weighted Average |
| 1.330 | 69 | 96.53% Pervious Area |
| 0.048 | 98 | 3.47% Impervious Area |

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Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 10/10/2024

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| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 14.1 | 100 | 0.0200 | 0.12 | | Sheet Flow, A Grass: Dense n= 0.240 P2= 3.30" |
| 2.2 | 337 | 0.0261 | 2.60 | | Shallow Concentrated Flow, B Unpaved Kv= 16.1 fps |
| 16.3 | 437 | Total | | | |

Summary for Subcatchment 22: WPre-03

Runoff = 8.77 cfs @ 12.13 hrs, Volume= 0.687 af, Depth= 4.54"
Routed to Link 25 : DP-2: Wetland A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.194 | 74 | >75% Grass cover, Good, HSG C |
| 1.510 | 65 | Brush, Good, HSG C |
| 0.034 | 98 | Impervious, HSG C |
| 0.045 | 98 | Roofs, HSG C |
| 0.032 | 70 | Woods, Good, HSG C |
| 1.815 | 67 | Weighted Average |
| 1.736 | 66 | 95.63% Pervious Area |
| 0.079 | 98 | 4.37% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 6.1 | 44 | 0.0318 | 0.12 | | Sheet Flow, A Grass: Dense n= 0.240 P2= 3.30" |
| 0.1 | 18 | 0.0278 | 3.38 | | Shallow Concentrated Flow, B Paved Kv= 20.3 fps |
| 2.6 | 392 | 0.0242 | 2.50 | | Shallow Concentrated Flow, C Unpaved Kv= 16.1 fps |
| 8.8 | 454 | Total | | | |

Summary for Subcatchment 23: WPre-04

Runoff = 1.37 cfs @ 12.19 hrs, Volume= 0.123 af, Depth= 4.30"
Routed to Link 25 : DP-2: Wetland A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.012 | 74 | >75% Grass cover, Good, HSG C |
| 0.332 | 65 | Brush, Good, HSG C |
| 0.344 | 65 | Weighted Average |
| 0.344 | 65 | 100.00% Pervious Area |

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Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 10/10/2024

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| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 12.1 | 100 | 0.0290 | 0.14 | | Sheet Flow, A Grass: Dense n= 0.240 P2= 3.30" |
| 1.1 | 145 | 0.0193 | 2.24 | | Shallow Concentrated Flow, B Unpaved Kv= 16.1 fps |
| 13.2 | 245 | Total | | | |

Summary for Subcatchment 24: WPre-05

Runoff = 2.46 cfs @ 12.08 hrs, Volume= 0.184 af, Depth= 6.94"
Routed to Link 25 : DP-2: Wetland A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.136 | 74 | >75% Grass cover, Good, HSG C |
| 0.000 | 65 | Brush, Good, HSG C |
| 0.001 | 98 | Impervious, HSG C |
| 0.177 | 98 | Offsite Impervious, HSG C |
| 0.004 | 70 | Woods, Good, HSG C |
| 0.318 | 87 | Weighted Average |
| 0.140 | 74 | 44.08% Pervious Area |
| 0.178 | 98 | 55.92% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

Summary for Link 25: DP-2: Wetland A

Inflow Area = 3.855 ac, 7.91% Impervious, Inflow Depth = 4.84" for 100-Year event
Inflow = 16.87 cfs @ 12.14 hrs, Volume= 1.556 af
Primary = 16.87 cfs @ 12.14 hrs, Volume= 1.556 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

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Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 1/17/2025

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Pond 1P: Lot 1 WQ Drywell Peak Elev=103.62' Storage=0.002 af Inflow=0.40 cfs 0.033 af
 Discarded=0.01 cfs 0.013 af Primary=0.33 cfs 0.020 af Outflow=0.34 cfs 0.033 af

Pond 2P: Lot 2 WQ Drywell Peak Elev=96.23' Storage=0.006 af Inflow=0.40 cfs 0.033 af
 Discarded=0.01 cfs 0.013 af Primary=0.20 cfs 0.020 af Outflow=0.21 cfs 0.033 af

Pond 3P: Lot 3 WQ Drywell Peak Elev=97.39' Storage=0.002 af Inflow=0.40 cfs 0.033 af
 Discarded=0.01 cfs 0.013 af Primary=0.34 cfs 0.020 af Outflow=0.34 cfs 0.033 af

Pond 4P: Lot 4 WQ Drywell Peak Elev=98.41' Storage=0.002 af Inflow=0.40 cfs 0.033 af
 Discarded=0.01 cfs 0.014 af Primary=0.34 cfs 0.018 af Outflow=0.35 cfs 0.033 af

Pond 5P: Lot 5 WQ Drywell Peak Elev=100.12' Storage=0.002 af Inflow=0.40 cfs 0.033 af
 Discarded=0.01 cfs 0.014 af Primary=0.33 cfs 0.019 af Outflow=0.34 cfs 0.033 af

Subcatchment 101: WPost-01 Runoff Area=0.079 ac 19.72% Impervious Runoff Depth=5.98"
 Tc=6.0 min CN=79 Runoff=0.54 cfs 0.039 af

Link 102: DP-1: Saugatucket Road - West Inflow=0.54 cfs 0.039 af
 Primary=0.54 cfs 0.039 af

Subcatchment 201: WPost-02 Runoff Area=1.479 ac 3.22% Impervious Runoff Depth=5.26"
 Flow Length=239' Tc=10.9 min CN=73 Runoff=7.73 cfs 0.648 af

Subcatchment 202: WPost-03 Runoff Area=0.361 ac 50.91% Impervious Runoff Depth=6.82"
 Tc=6.0 min CN=86 Runoff=2.75 cfs 0.205 af

Subcatchment 203: WPost-04 Runoff Area=1.821 ac 27.95% Impervious Runoff Depth=6.22"
 Flow Length=165' Tc=15.8 min CN=81 Runoff=9.66 cfs 0.943 af

Pond 204: Forebay A Peak Elev=96.47' Storage=1,735 cf Inflow=9.66 cfs 0.943 af
 Primary=0.36 cfs 0.049 af Secondary=8.97 cfs 0.894 af Outflow=9.22 cfs 0.943 af

Subcatchment 205: WPost-05 Runoff Area=0.059 ac 0.00% Impervious Runoff Depth=5.38"
 Tc=0.0 min CN=74 Runoff=0.45 cfs 0.026 af

Pond 206: WQ Infiltration Pond A Peak Elev=96.51' Storage=1,972 cf Inflow=0.53 cfs 0.076 af
 Discarded=0.03 cfs 0.075 af Primary=0.02 cfs 0.001 af Outflow=0.05 cfs 0.076 af

Subcatchment 207: WPost-06 Runoff Area=0.154 ac 0.00% Impervious Runoff Depth=5.38"
 Tc=0.0 min CN=74 Runoff=1.18 cfs 0.069 af

Pond 208: Infiltration Pond A Peak Elev=96.43' Storage=6,701 cf Inflow=9.35 cfs 0.963 af
 Discarded=0.10 cfs 0.200 af Primary=8.90 cfs 0.763 af Outflow=8.99 cfs 0.963 af

Link 209: DP-2: Wetland A Inflow=16.52 cfs 1.616 af
 Primary=16.52 cfs 1.616 af

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Type III 24-hr 100-Year Rainfall=8.50"

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| | |
|------------------------------------|---|
| Subcatchment L1: Lot 1 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=8.26" Tc=6.0 min CN=98 Runoff=0.40 cfs 0.033 af |
| Subcatchment L2: Lot 2 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=8.26" Tc=6.0 min CN=98 Runoff=0.40 cfs 0.033 af |
| Subcatchment L3: Lot 3 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=8.26" Tc=6.0 min CN=98 Runoff=0.40 cfs 0.033 af |
| Subcatchment L4: Lot 4 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=8.26" Tc=6.0 min CN=98 Runoff=0.40 cfs 0.033 af |
| Subcatchment L5: Lot 5 Roof | Runoff Area=2,076 sf 100.00% Impervious Runoff Depth=8.26" Tc=6.0 min CN=98 Runoff=0.40 cfs 0.033 af |

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Type III 24-hr 100-Year Rainfall=8.50"

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Summary for Pond 1P: Lot 1 WQ Drywell

Inflow Area = 0.048 ac, 100.00% Impervious, Inflow Depth = 8.26" for 100-Year event
 Inflow = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af
 Outflow = 0.34 cfs @ 12.13 hrs, Volume= 0.033 af, Atten= 15%, Lag= 2.9 min
 Discarded = 0.01 cfs @ 7.63 hrs, Volume= 0.013 af
 Primary = 0.33 cfs @ 12.13 hrs, Volume= 0.020 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Peak Elev= 103.62' @ 12.13 hrs Surf.Area= 0.007 ac Storage= 0.002 af

Plug-Flow detention time= 28.3 min calculated for 0.033 af (100% of inflow)
 Center-of-Mass det. time= 28.3 min (768.8 - 740.5)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|---|
| #1 | 101.50' | 0.001 af | 18.00'W x 18.00'L x 0.50'H Drywell 0.004 af Overall x 33.3% Voids |
| #2 | 103.00' | 0.002 af | 9.00'W x 9.00'L x 1.00'H Above Drywell -Impervious |
| | | 0.003 af | Total Available Storage |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|---------|--|
| #1 | Discarded | 101.50' | 1.055 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 103.00' | 4.00" Horiz. 4" Outlet C= 0.600 Limited to weir flow at low heads |

Discarded OutFlow Max=0.01 cfs @ 7.63 hrs HW=101.53' (Free Discharge)

↑**1=Exfiltration** (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=0.33 cfs @ 12.13 hrs HW=103.62' (Free Discharge)

↑**2=4" Outlet** (Orifice Controls 0.33 cfs @ 3.80 fps)

Summary for Pond 2P: Lot 2 WQ Drywell

Inflow Area = 0.048 ac, 100.00% Impervious, Inflow Depth = 8.26" for 100-Year event
 Inflow = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af
 Outflow = 0.21 cfs @ 12.21 hrs, Volume= 0.033 af, Atten= 47%, Lag= 7.7 min
 Discarded = 0.01 cfs @ 7.35 hrs, Volume= 0.013 af
 Primary = 0.20 cfs @ 12.21 hrs, Volume= 0.020 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Peak Elev= 96.23' @ 12.21 hrs Surf.Area= 0.008 ac Storage= 0.006 af

Plug-Flow detention time= 41.2 min calculated for 0.033 af (100% of inflow)
 Center-of-Mass det. time= 41.2 min (781.7 - 740.5)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|---|
| #1 | 94.50' | 0.001 af | 11.00'W x 30.00'L x 0.50'H Drywell 0.004 af Overall x 33.3% Voids |
| #2 | 96.00' | 0.010 af | 30.00'W x 30.00'L x 0.50'H Above Drywell -Impervious |
| | | 0.012 af | Total Available Storage |

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Type III 24-hr 100-Year Rainfall=8.50"

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| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|--|
| #1 | Discarded | 94.50' | 0.990 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 96.00' | 4.00" Horiz. 4" Outlet C= 0.600 Limited to weir flow at low heads |

Discarded OutFlow Max=0.01 cfs @ 7.35 hrs HW=94.52' (Free Discharge)↑**1=Exfiltration** (Exfiltration Controls 0.01 cfs)**Primary OutFlow** Max=0.20 cfs @ 12.21 hrs HW=96.23' (Free Discharge)↑**2=4" Outlet** (Orifice Controls 0.20 cfs @ 2.31 fps)**Summary for Pond 3P: Lot 3 WQ Drywell**

Inflow Area = 0.048 ac, 100.00% Impervious, Inflow Depth = 8.26" for 100-Year event
 Inflow = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af
 Outflow = 0.34 cfs @ 12.13 hrs, Volume= 0.033 af, Atten= 13%, Lag= 2.8 min
 Discarded = 0.01 cfs @ 7.82 hrs, Volume= 0.013 af
 Primary = 0.34 cfs @ 12.13 hrs, Volume= 0.020 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Peak Elev= 97.39' @ 12.13 hrs Surf.Area= 0.008 ac Storage= 0.002 af

Plug-Flow detention time= 30.0 min calculated for 0.033 af (100% of inflow)

Center-of-Mass det. time= 30.0 min (770.4 - 740.5)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|---|
| #1 | 94.25' | 0.001 af | 11.00'W x 30.00'L x 0.50'H Drywell 0.004 af Overall x 33.3% Voids |
| #2 | 96.75' | 0.003 af | 9.00'W x 8.00'L x 2.00'H Above Drywell -Impervious |
| | | 0.005 af | Total Available Storage |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|--|
| #1 | Discarded | 94.25' | 0.990 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 96.75' | 4.00" Horiz. 4" Outlet C= 0.600 Limited to weir flow at low heads |

Discarded OutFlow Max=0.01 cfs @ 7.82 hrs HW=94.30' (Free Discharge)↑**1=Exfiltration** (Exfiltration Controls 0.01 cfs)**Primary OutFlow** Max=0.34 cfs @ 12.13 hrs HW=97.39' (Free Discharge)↑**2=4" Outlet** (Orifice Controls 0.34 cfs @ 3.86 fps)**Summary for Pond 4P: Lot 4 WQ Drywell**

Inflow Area = 0.048 ac, 100.00% Impervious, Inflow Depth = 8.26" for 100-Year event
 Inflow = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af
 Outflow = 0.35 cfs @ 12.13 hrs, Volume= 0.033 af, Atten= 12%, Lag= 2.6 min
 Discarded = 0.01 cfs @ 8.50 hrs, Volume= 0.014 af
 Primary = 0.34 cfs @ 12.13 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

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Type III 24-hr 100-Year Rainfall=8.50"

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Peak Elev= 98.41' @ 12.13 hrs Surf.Area= 0.007 ac Storage= 0.002 af

Plug-Flow detention time= 23.5 min calculated for 0.033 af (100% of inflow)
Center-of-Mass det. time= 23.5 min (764.0 - 740.5)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|---|
| #1 | 96.25' | 0.001 af | 18.00'W x 18.00'L x 0.50'H Drywell 0.004 af Overall x 33.3% Voids |
| #2 | 97.75' | 0.003 af | 8.00'W x 8.00'L x 2.00'H Above Drywell -Impervious |
| | | 0.004 af | Total Available Storage |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|--|
| #1 | Discarded | 96.25' | 1.280 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 97.75' | 4.00" Horiz. 4" Outlet C= 0.600 Limited to weir flow at low heads |

Discarded OutFlow Max=0.01 cfs @ 8.50 hrs HW=96.29' (Free Discharge)

↑**1=Exfiltration** (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=0.34 cfs @ 12.13 hrs HW=98.41' (Free Discharge)

↑**2=4" Outlet** (Orifice Controls 0.34 cfs @ 3.90 fps)

Summary for Pond 5P: Lot 5 WQ Drywell

Inflow Area = 0.048 ac, 100.00% Impervious, Inflow Depth = 8.26" for 100-Year event
 Inflow = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af
 Outflow = 0.34 cfs @ 12.13 hrs, Volume= 0.033 af, Atten= 15%, Lag= 2.9 min
 Discarded = 0.01 cfs @ 8.19 hrs, Volume= 0.014 af
 Primary = 0.33 cfs @ 12.13 hrs, Volume= 0.019 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Peak Elev= 100.12' @ 12.13 hrs Surf.Area= 0.007 ac Storage= 0.002 af

Plug-Flow detention time= 24.9 min calculated for 0.033 af (100% of inflow)
Center-of-Mass det. time= 24.8 min (765.3 - 740.5)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|---|
| #1 | 98.00' | 0.001 af | 18.00'W x 18.00'L x 0.50'H Drywell 0.004 af Overall x 33.3% Voids |
| #2 | 99.50' | 0.002 af | 9.00'W x 9.00'L x 1.00'H Above Drywell -Impervious |
| | | 0.003 af | Total Available Storage |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|--|
| #1 | Discarded | 98.00' | 1.215 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 99.50' | 4.00" Horiz. 4" Outlet C= 0.600 Limited to weir flow at low heads |

Discarded OutFlow Max=0.01 cfs @ 8.19 hrs HW=98.03' (Free Discharge)

↑**1=Exfiltration** (Exfiltration Controls 0.01 cfs)

Primary OutFlow Max=0.33 cfs @ 12.13 hrs HW=100.12' (Free Discharge)

↑**2=4" Outlet** (Orifice Controls 0.33 cfs @ 3.78 fps)

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Type III 24-hr 100-Year Rainfall=8.50"

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Summary for Subcatchment 101: WPost-01

Runoff = 0.54 cfs @ 12.09 hrs, Volume= 0.039 af, Depth= 5.98"

Routed to Link 102 : DP-1: Saugatucket Road - West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.063 | 74 | >75% Grass cover, Good, HSG C |
| 0.000 | 98 | Impervious, HSG C |
| 0.015 | 98 | Offsite Impervious, HSG C |
| 0.079 | 79 | Weighted Average |
| 0.063 | 74 | 80.28% Pervious Area |
| 0.016 | 98 | 19.72% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---------------|
| 6.0 | | | | | Direct Entry, |

Summary for Link 102: DP-1: Saugatucket Road - West

Inflow Area = 0.079 ac, 19.72% Impervious, Inflow Depth = 5.98" for 100-Year event

Inflow = 0.54 cfs @ 12.09 hrs, Volume= 0.039 af

Primary = 0.54 cfs @ 12.09 hrs, Volume= 0.039 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Subcatchment 201: WPost-02

Runoff = 7.73 cfs @ 12.15 hrs, Volume= 0.648 af, Depth= 5.26"

Routed to Link 209 : DP-2: Wetland A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 1.081 | 74 | >75% Grass cover, Good, HSG C |
| 0.280 | 65 | Brush, Good, HSG C |
| 0.048 | 98 | Roofs, HSG C |
| 0.070 | 70 | Woods, Good, HSG C |
| 1.479 | 73 | Weighted Average |
| 1.432 | 72 | 96.78% Pervious Area |
| 0.048 | 98 | 3.22% Impervious Area |

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Type III 24-hr 100-Year Rainfall=8.50"

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| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|-------------------------------------|
| 10.1 | 100 | 0.0460 | 0.17 | | Sheet Flow, A |
| | | | | | Grass: Dense n= 0.240 P2= 3.30" |
| 0.8 | 139 | 0.0315 | 2.86 | | Shallow Concentrated Flow, B |
| | | | | | Unpaved Kv= 16.1 fps |
| 10.9 | 239 | Total | | | |

Summary for Subcatchment 202: WPost-03

Runoff = 2.75 cfs @ 12.08 hrs, Volume= 0.205 af, Depth= 6.82"
 Routed to Link 209 : DP-2: Wetland A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.150 | 74 | >75% Grass cover, Good, HSG C |
| 0.027 | 65 | Brush, Good, HSG C |
| 0.003 | 98 | Impervious, HSG C |
| 0.180 | 98 | Offsite Impervious, HSG C |
| 0.361 | 86 | Weighted Average |
| 0.177 | 73 | 49.09% Pervious Area |
| 0.184 | 98 | 50.91% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

Summary for Subcatchment 203: WPost-04

Runoff = 9.66 cfs @ 12.21 hrs, Volume= 0.943 af, Depth= 6.22"
 Routed to Pond 204 : Forebay A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 1.312 | 74 | >75% Grass cover, Good, HSG C |
| 0.318 | 98 | Impervious, HSG C |
| 0.191 | 98 | Roofs, HSG C |
| 1.821 | 81 | Weighted Average |
| 1.312 | 74 | 72.05% Pervious Area |
| 0.509 | 98 | 27.95% Impervious Area |

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| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|-------------------------------------|
| 15.4 | 100 | 0.0160 | 0.11 | | Sheet Flow, A |
| | | | | | Grass: Dense n= 0.240 P2= 3.30" |
| 0.4 | 65 | 0.0368 | 3.09 | | Shallow Concentrated Flow, B |
| | | | | | Unpaved Kv= 16.1 fps |
| 15.8 | 165 | Total | | | |

Summary for Pond 204: Forebay A

Inflow Area = 1.821 ac, 27.95% Impervious, Inflow Depth = 6.22" for 100-Year event
 Inflow = 9.66 cfs @ 12.21 hrs, Volume= 0.943 af
 Outflow = 9.22 cfs @ 12.23 hrs, Volume= 0.943 af, Atten= 5%, Lag= 1.1 min
 Primary = 0.36 cfs @ 12.17 hrs, Volume= 0.049 af
 Routed to Pond 206 : WQ Infiltration Pond A
 Secondary = 8.97 cfs @ 12.24 hrs, Volume= 0.894 af
 Routed to Pond 208 : Infiltration Pond A

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Automatic Starting Elev= 95.00' Surf.Area= 311 sf Storage= 376 cf
 Peak Elev= 96.47' @ 12.29 hrs Surf.Area= 1,849 sf Storage= 1,735 cf (1,359 cf above start)

Plug-Flow detention time= 25.2 min calculated for 0.934 af (99% of inflow)
 Center-of-Mass det. time= 15.9 min (823.3 - 807.4)

| Volume | Invert | Avail.Storage | Storage Description | | | |
|------------------|-------------------|---------------|--|------------------------|------------------|--|
| #1 | 93.00' | 2,990 cf | Custom Stage Data (Irregular) Listed below (Recalc) | | | |
| Elevation (feet) | Surf.Area (sq-ft) | Perim. (feet) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) | |
| 93.00 | 88 | 43.1 | 0 | 0 | 88 | |
| 95.00 | 311 | 310.8 | 376 | 376 | 7,635 | |
| 96.00 | 1,118 | 248.0 | 673 | 1,049 | 10,442 | |
| 97.00 | 2,904 | 393.0 | 1,941 | 2,990 | 17,845 | |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 95.00' | 6.00" Round Culverts X 3.00 L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 95.00' / 94.50' S= 0.0250 '/ Cc= 0.900 n= 0.012, Flow Area= 0.20 sf |
| #2 | Secondary | 95.65' | 10.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |

Primary OutFlow Max=0.24 cfs @ 12.17 hrs HW=96.38' TW=96.37' (Dynamic Tailwater)
 ↑**1=Culverts** (Inlet Controls 0.24 cfs @ 0.41 fps)

Secondary OutFlow Max=8.41 cfs @ 12.24 hrs HW=96.45' TW=96.41' (Dynamic Tailwater)
 ↑**2=Broad-Crested Rectangular Weir** (Weir Controls 8.41 cfs @ 1.05 fps)

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Summary for Subcatchment 205: WPost-05

Runoff = 0.45 cfs @ 12.00 hrs, Volume= 0.026 af, Depth= 5.38"
 Routed to Pond 206 : WQ Infiltration Pond A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.059 | 74 | >75% Grass cover, Good, HSG C |
| 0.059 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 0.0 | | | | | Direct Entry, |

Summary for Pond 206: WQ Infiltration Pond A

Inflow Area = 1.880 ac, 27.07% Impervious, Inflow Depth = 0.48" for 100-Year event
 Inflow = 0.53 cfs @ 12.17 hrs, Volume= 0.076 af
 Outflow = 0.05 cfs @ 12.57 hrs, Volume= 0.076 af, Atten= 91%, Lag= 24.2 min
 Discarded = 0.03 cfs @ 12.57 hrs, Volume= 0.075 af
 Primary = 0.02 cfs @ 12.57 hrs, Volume= 0.001 af
 Routed to Pond 208 : Infiltration Pond A

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Peak Elev= 96.51' @ 12.57 hrs Surf.Area= 1,339 sf Storage= 1,972 cf

Plug-Flow detention time= 659.9 min calculated for 0.076 af (100% of inflow)
 Center-of-Mass det. time= 659.9 min (1,453.1 - 793.2)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 94.50' | 2,675 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|------------------|-------------------|------------------------|------------------------|
| 94.50 | 626 | 0 | 0 |
| 97.00 | 1,514 | 2,675 | 2,675 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Discarded | 94.50' | 0.990 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 96.50' | 10.0' long x 14.5' breadth Overflow Weir |
| | | | Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 |
| | | | Coef. (English) 2.66 2.69 2.70 2.65 2.63 2.65 2.64 2.63 |

Discarded OutFlow Max=0.03 cfs @ 12.57 hrs HW=96.51' (Free Discharge)
 ↑**1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.02 cfs @ 12.57 hrs HW=96.51' TW=96.25' (Dynamic Tailwater)
 ↑**2=Overflow Weir** (Weir Controls 0.02 cfs @ 0.23 fps)

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Summary for Subcatchment 207: WPost-06

Runoff = 1.18 cfs @ 12.00 hrs, Volume= 0.069 af, Depth= 5.38"
 Routed to Pond 208 : Infiltration Pond A

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 0.154 | 74 | >75% Grass cover, Good, HSG C |
| 0.154 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 0.0 | | | | | Direct Entry, |

Summary for Pond 208: Infiltration Pond A

Inflow Area = 2.034 ac, 25.03% Impervious, Inflow Depth = 5.68" for 100-Year event
 Inflow = 9.35 cfs @ 12.24 hrs, Volume= 0.963 af
 Outflow = 8.99 cfs @ 12.29 hrs, Volume= 0.963 af, Atten= 4%, Lag= 3.2 min
 Discarded = 0.10 cfs @ 12.29 hrs, Volume= 0.200 af
 Primary = 8.90 cfs @ 12.29 hrs, Volume= 0.763 af
 Routed to Link 209 : DP-2: Wetland A

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Peak Elev= 96.43' @ 12.29 hrs Surf.Area= 4,172 sf Storage= 6,701 cf

Plug-Flow detention time= 129.2 min calculated for 0.963 af (100% of inflow)
 Center-of-Mass det. time= 129.3 min (953.4 - 824.2)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 94.50' | 9,194 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|------------------|-------------------|------------------------|------------------------|
| 94.50 | 2,769 | 0 | 0 |
| 97.00 | 4,586 | 9,194 | 9,194 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|--|
| #1 | Discarded | 94.50' | 0.990 in/hr Exfiltration over Surface area Phase-In= 0.01' |
| #2 | Primary | 95.75' | 5.0' long x 0.5' breadth Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |

Discarded OutFlow Max=0.10 cfs @ 12.29 hrs HW=96.43' (Free Discharge)
 ↑1=Exfiltration (Exfiltration Controls 0.10 cfs)

Primary OutFlow Max=8.90 cfs @ 12.29 hrs HW=96.43' TW=0.00' (Dynamic Tailwater)
 ↑2=Weir (Weir Controls 8.90 cfs @ 2.61 fps)

Summary for Link 209: DP-2: Wetland A

Inflow Area = 3.873 ac, 19.11% Impervious, Inflow Depth = 5.01" for 100-Year event
 Inflow = 16.52 cfs @ 12.18 hrs, Volume= 1.616 af
 Primary = 16.52 cfs @ 12.18 hrs, Volume= 1.616 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Subcatchment L1: Lot 1 Roof

Runoff = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 8.26"
 Routed to Pond 1P : Lot 1 WQ Drywell

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,076 | 98 | Roofs, HSG C |
| 2,076 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

Summary for Subcatchment L2: Lot 2 Roof

Runoff = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 8.26"
 Routed to Pond 2P : Lot 2 WQ Drywell

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,076 | 98 | Roofs, HSG C |
| 2,076 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

Summary for Subcatchment L3: Lot 3 Roof

Runoff = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 8.26"
 Routed to Pond 3P : Lot 3 WQ Drywell

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

3287-001-ALLS-PHCD-INHS

Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 1/17/2025

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| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,076 | 98 | Roofs, HSG C |
| 2,076 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

Summary for Subcatchment L4: Lot 4 Roof

Runoff = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 8.26"
Routed to Pond 4P : Lot 4 WQ Drywell

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,076 | 98 | Roofs, HSG C |
| 2,076 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

Summary for Subcatchment L5: Lot 5 Roof

Runoff = 0.40 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 8.26"
Routed to Pond 5P : Lot 5 WQ Drywell

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Type III 24-hr 100-Year Rainfall=8.50"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,076 | 98 | Roofs, HSG C |
| 2,076 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|----------------------|
| 6.0 | | | | | Direct Entry, |

A3.5.4.6 HydroCAD 100-Year Emergency Outlet Calculations

Summary for Pond 208: Infiltration Pond A

Inflow Area = 2.034 ac, 25.03% Impervious, Inflow Depth = 5.67" for 100-Year event
 Inflow = 9.36 cfs @ 12.23 hrs, Volume= 0.961 af
 Outflow = 9.01 cfs @ 12.29 hrs, Volume= 0.869 af, Atten= 4%, Lag= 3.2 min
 Primary = 9.01 cfs @ 12.29 hrs, Volume= 0.869 af
 Routed to Link 209 : DP-2: Wetland A

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Peak Elev= 96.44' @ 12.29 hrs Surf.Area= 4,176 sf Storage= 6,722 cf

Plug-Flow detention time= 75.8 min calculated for 0.869 af (90% of inflow)
 Center-of-Mass det. time= 28.8 min (851.8 - 823.1)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 94.50' | 9,194 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|---------------------|----------------------|---------------------------|---------------------------|
| 94.50 | 2,769 | 0 | 0 |
| 97.00 | 4,586 | 9,194 | 9,194 |

| Device | Routing | Invert | Outlet Devices |
|--------|---------|--------|--|
| #1 | Primary | 95.75' | 5.0' long x 0.5' breadth Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |

Primary OutFlow Max=9.01 cfs @ 12.29 hrs HW=96.44' TW=0.00' (Dynamic Tailwater)
 ↑**1=Weir** (Weir Controls 9.01 cfs @ 2.63 fps)

Appendix B – Mounding Calculations

DiPrete Engineering has prepared groundwater mounding calculations for the proposed infiltration pond. The infiltration pond has been designed to infiltrate stormwater as well as release stormwater through a weir.

DiPrete Engineering has calculated the groundwater mounding using the USGS Hantush Calculator. The calculator is available online at <http://pubs.usgs.gov/sir/2010/5102/>.

The calculator provided by the USGS requires several variables:

R – Recharge infiltration rate (feet/day):

Recharge rate is the vertical conductivity (Kv) of the soil. The vertical conductivity was determined based on soil texture and table 5-3 in section 5.3.4 of the RISDISM of the RISDISM. A value of 0.99 in/hr or 1.98 ft/day has been used for these calculations.

Sy – Specific Yield:

Specific Yield is specific to the parent material through which the infiltration occurs. Onsite soil evaluations classified the soils as silt. A value for Sy has been obtained from Table 4.3 of Hydrology and Hydraulic Systems by Ram S. Gupta:

**TABLE 4.3 REPRESENTATIVE VALUES
OF SPECIFIC YIELD FOR SOILS AND ROCKS**

| Material | Specific Yield (%) |
|----------------------------|--------------------|
| Gravel, coarse | 23 |
| Gravel, medium | 24 |
| Gravel, fine | 25 |
| Sand, coarse | 27 |
| Sand, medium | 28 |
| Sand, fine | 23 |
| Silt | 8 |
| Clay | 3 |
| Sandstone, fine-grained | 21 |
| Sandstone, medium-grained | 27 |
| Limestone | 14 |
| Dune sand | 38 |
| Loess | 18 |
| Peat | 44 |
| Schist | 26 |
| Siltstone | 12 |
| Till, predominantly silt | 6 |
| Till, predominantly sand | 16 |
| Till, predominantly gravel | 16 |
| Tuff | 21 |

Source: Todd, 1980.

HYDROLOGY
&
HYDRAULIC
SYSTEMS

RAM S. GUPTA, P.E., P.E.
Rajiv Gandhi University, Bhopal, M.P.
Civil Engineer, Inc., Bhopal, M.P.

K – Hydraulic conductivity, Kh (feet/day):

Mounding calculations require the hydraulic conductivity (Kh) value of the soils. According to USGS SIR 2010-5102, Vertical Conductivity is approximately 1/10 of horizontal conductivity. The vertical conductivity was determined based on infiltration tests. The vertical conductivity is 0.99 in/hr, which equates to a horizontal conductivity of 9.9 in/hr or 19.8 ft/day.

x & y – ½ of the basin length:

The x and y variables represent the length and width of the system. The overall system is approximately 84' x 33' and the ½ basin length and width is 42' x 16.5'.

t – Duration of infiltration period in (days):

The time of infiltration is calculated from volume infiltrated divided by the square footage of the pond and the infiltration rate (Kv).

| Volume Infiltrated (af) | Pond Infiltrating Surface Area (sf) | Infiltration Rate (ft/day) | T (days) |
|-------------------------|-------------------------------------|----------------------------|----------|
| 0.202 | 2,769 | 0.99 | 1.7 |

hi(0) – initial thickness of saturated zone (feet):

The initial thickness of the saturated zone is the depth from the water table to the impervious limiting layer. Test holes performed did not encounter ledge. Test holes reached a total depth of 10'. To be conservative, the impervious limiting layer is considered to be the bottom of the test hole. Ledge could be significantly deeper in the area of the infiltration pond, but based on available data we have assumed the bottom of the test hole.

Conclusion:

| System Bottom | System Top | 100-Year Mound height (ft) | 100-Year Mound Elevation | 25-Year Mound height (ft) | 25-Year Mound Elevation |
|---------------|------------|----------------------------|--------------------------|---------------------------|-------------------------|
| 94.50 | 97.50 | 4.41 | 96.91 | 4.31 | 96.81 |

The mounding height is obtained from the USGS Hantush Calculator. The mound elevation is determined by adding the mound height to the average seasonal high groundwater for each respective storm system.

During the 25- and 100-year storms the mound will come into the basin bottom for a short period during the storm event. DiPrete Engineering reviewed the infiltration pond calculations for larger storm events with no infiltration occurring. Since the infiltration pond has an outlet to the wetland, DiPrete Engineering reviewed the impacts to the wetland during all storm events. DiPrete Engineering determined that the peak runoff rate to the wetland for the 25- and 100-year storms remain mitigated when considering the reduced infiltration and volume which could be encountered should the groundwater mound enter the infiltration pond bottom. This is a conservative approach since the mound wouldn't instantly occur during the storm event and wouldn't last for the entire duration of the storm. This scenario is a worst-case scenario with larger storm events occurring at a time where the water table is at a seasonal high elevation.

The following table summarizes the results of the revised analysis for the Design Point:

| | 25-Year cfs rate | 100-Year cfs rate |
|------------------------------|------------------|-------------------|
| Pre Development | 9.80 | 16.87 |
| Post Development | 9.02 | 16.56 |
| Post Development Mounding | 9.32 | 16.71 |

The analysis shows only a slight increase in rate of discharge to the wetland, which remains below the pre-development peak rate. Additionally, the infiltration pond still remains with more than 1' of freeboard.

The other concern with the mound is the drain out time for the infiltration basin. The infiltration pond needs to drain out within 72 hours of the storm event. If there is no mound within the system, the infiltration pond drains out within 40 hours of the start of stormwater entering the basin. This means when the mound is within the system, there is approximately 32 hours for the mound to dissipate and the remainder of the stormwater to infiltrate. Note the system outlet is at 95.75 with the bottom of the basin at elevation 94.50. That means there is 1.25' of stormwater (about 4,067 cf) of stormwater that needs to infiltrate in 32 hours in a silty loam soil. It is not anticipated that stormwater will remain in the system for longer than 72 hours after the 100-year storm event.

In summary, the ground water mound will not have a detrimental effect to the functionality of the infiltration pond and there will not be an impact to the wetland due to the groundwater mound. See attached Mounding Calculation Sheets and HydroCAD.

Appendix C – Floodplain Study

Although the project site is not within any FEMA 100-year floodplain, a floodplain analysis was conducted to assess if Indian Run Brook could flood into the project area during the 100-year storm event.

The study area is the section of Indian Run brook that runs through the southeast corner of the property. The drainage area, cover types, and Time of Concentration (Tc) were determined using StreamStats and modeled in HydroCAD. The acreage of woods, impervious, water, and wetlands was determined using the StreamStats report. The remaining area was assigned as grass. Upland areas were assigned HSG C according to Web Soil Survey. Water and wetland areas were assigned HSG D. A direct entry Tc was used in HydroCAD. The length of time was assigned so that the 100-year discharge rate of the subcatchment in HydroCAD matched the 100-year discharge rate reported in StreamStats. The section of Indian Run Brook that runs through the property was modeled as a reach in HydroCAD using existing topography in AutoCAD.

During the 100-year storm event, the section of Indian Run Brook within the site's property floods 1.16 feet. At the highest point of the stream within the property boundary, this floods to approximately elevation 88.16. As the A-Series wetland boundary roughly follows elevation 90, the floodplain of Indian Run Brook does not encroach into the defined project area.

StreamStats Report

Region ID: RI

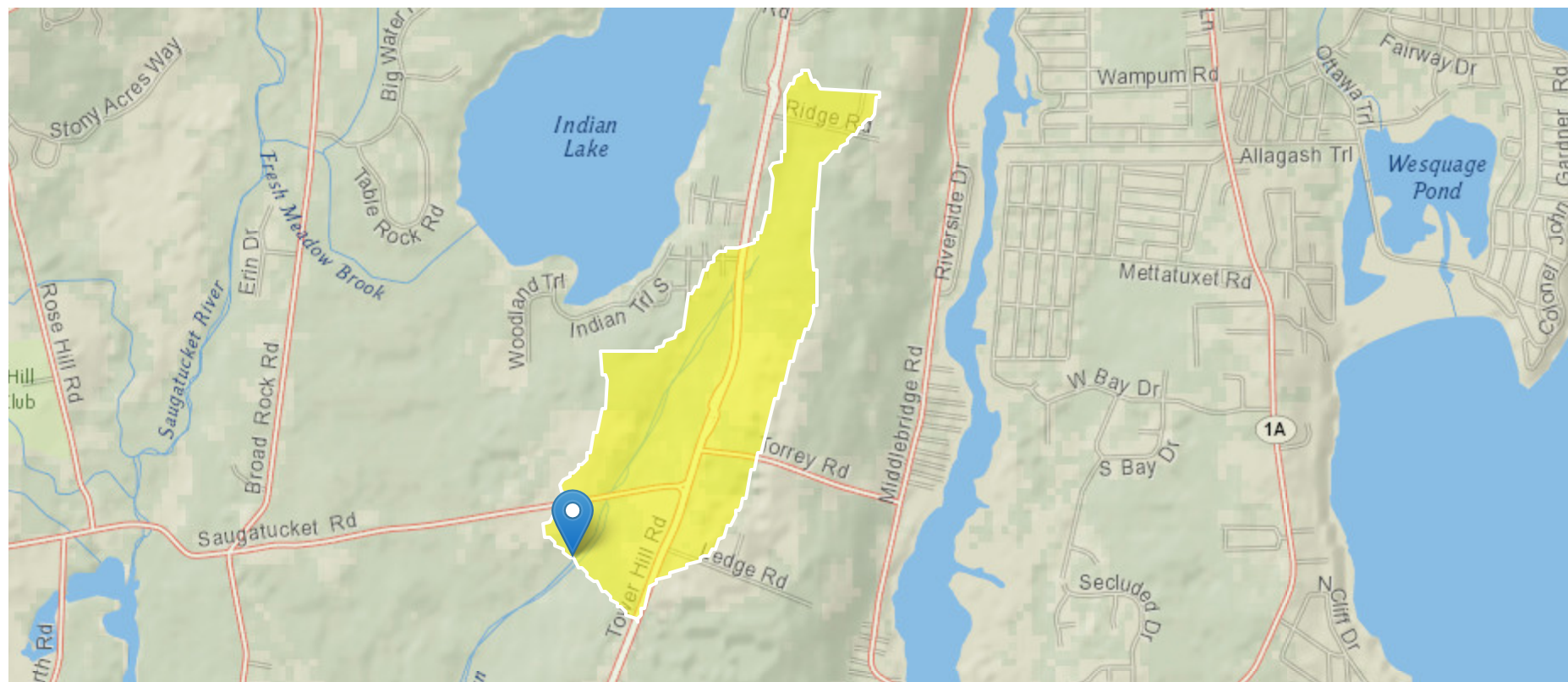
Workspace ID: RI20250116145254174000

Clicked Point (Latitude, Longitude): 41.46352, -71.46943

NHD Stream GNIS Name of Click Point:  Indian Run

HUC 8 of Clicked Point: 01090006 (Point Judith-Block Island)

Time: 2025-01-16 09:53:22 -0500



 Collapse All

➤ Basin Characteristics

| Parameter Code | Parameter Description | Value | Unit | |
|----------------|---|-------|---------------|--------------|
| CAT1ROADS | Length of interstates lmtd access highways and ramps for lmtd access highways, includes cloverleaf interchanges (USGS Ntl Transp Dataset) | 0 | miles | |
| CAT2ROADS | Length of sec hwy or maj connecting roads; main arteries & hwys not lmtd access, usually in the US Hwy or State Hwy systems (USGS Ntl Transp Dataset) | 2 | miles | |
| CAT3ROADS | Length of local connecting roads; roads that collect traffic from local roads & connect towns, subdivisions & neighborhoods (USGS Nat Transp Dataset) | 0 | miles | |
| CAT4ROADS | Length of local roads; generally paved street, road, or byway that usually have single lane of traffic in each direction (USGS Ntnl Transp Dataset) | 1.76 | miles | |
| CROPS | Percent of area covered by agriculture | 15.4 | percent | |
| CROSCOUNT1 | Number of intersections between streams and roads, where the roads are interstate, limited access highway, or ramp (CAT1ROADS) | 0 | dimensionless | |
| CROSCOUNT2 | Number of intersections between streams and roads, where the roads are secondary highway or major connecting road (CAT2ROADS) | 2 | dimensionless | |
| CROSCOUNT3 | Number of intersections between streams and roads, where roads are local connecting roads (CAT3ROADS) | 0 | dimensionless | |
| CROSCOUNT4 | Number of intersections between streams and roads, where roads are local roads (CAT4ROADS) | 1 | dimensionless | |
| CRSDFT | Percentage of area of coarse-grained stratified drift | 0 | percent | |
| CSL10_85 | Change in elevation divided by length between points 10 and 85 percent of distance along main channel to basin divide - main channel method not known | 34.5 | feet per mi | |
| DRNAREA | Area that drains to a point on a stream | 0.43 | square miles | 275.2 acres |
| ELEV | Mean Basin Elevation | 135 | feet | |
| FOREST | Percentage of area covered by forest | 24.9 | percent | 68.525 acres |

| Parameter Code | Parameter Description | Value | Unit |
|----------------|---|-------|-----------------------|
| LC11DEV | Percentage of developed (urban) land from NLCD 2011 classes 21-24 | 29.5 | percent |
| LC11IMP | Average percentage of impervious area determined from NLCD 2011 impervious dataset | 10.3 | percent |
| LFPLENGTH | Length of longest flow path | 1.79 | miles |
| STORNHD | Percent storage (wetlands and waterbodies) determined from 1:24K NHD | 7.9 | percent |
| STRDEN | Stream Density -- total length of streams divided by drainage area | 2.29 | miles per square mile |
| STRDENED | Stream Density -- total length of streams divided by drainage area, edited from NHD | 2.29 | miles per square mile |
| STRMTOT | total length of all mapped streams (1:24,000-scale) in the basin | 0.98 | miles |
| STRMTOTED | Total stream length in miles - edited NHD | 0.98 | miles |
| WATER | Percent of area covered by open water (lakes, ponds, reservoirs) | 0.27 | percent |
| WETLAND | Percentage of Wetlands | 33.8 | percent |

28.346 acres

0.743 acres

93.018 acres

REMAINDER GRASS: 84.568 ac

➤ Peak-Flow Statistics

Peak-Flow Statistics Parameters [Statewide peak 2012 5109]

| Parameter Code | Parameter Name | Value | Units | Min Limit | Max Limit |
|----------------|--------------------------|-------|-----------------------|-----------|-----------|
| DRNAREA | Drainage Area | 0.43 | square miles | 4 | 404 |
| STORNHD | Percent Storage from NHD | 7.9 | percent | 3.37 | 19 |
| STRDEN | Stream Density | 2.29 | miles per square mile | 1.25 | 3.53 |

Peak-Flow Statistics Disclaimers [Statewide peak 2012 5109]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors.

Peak-Flow Statistics Flow Report [Statewide peak 2012 5109]

| Statistic | Value | Unit |
|-----------------------|-------|--------------------|
| 20-percent AEP flood | 20.6 | ft ³ /s |
| 10-percent AEP flood | 26.8 | ft ³ /s |
| 4-percent AEP flood | 37.6 | ft ³ /s |
| 2-percent AEP flood | 46.5 | ft ³ /s |
| 1-percent AEP flood | 56.4 | ft ³ /s |
| 0.5-percent AEP flood | 66 | ft ³ /s |
| 0.2-percent AEP flood | 79.9 | ft ³ /s |

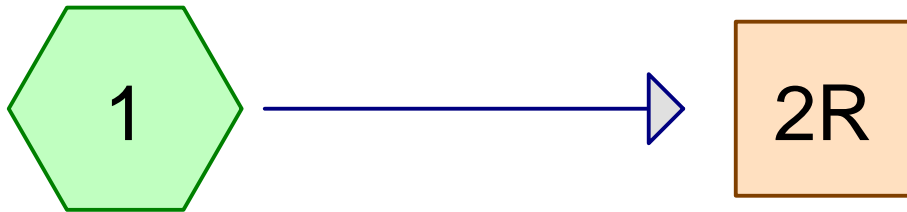
Peak-Flow Statistics Citations

Zarriello, P.J., Ahearn, E.A., and Levin, S.B., 2012, Magnitude of flood flows for selected annual exceedance probabilities in Rhode Island through 2010: U.S. Geological Survey Scientific Investigations Report 2012–5109, 93 p. (<http://pubs.usgs.gov/sir/2012/5109>)

➤ Low-Flow Statistics

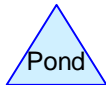
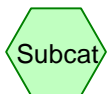
Low-Flow Statistics Parameters [Statewide Low Flow 2014 5010]

| Parameter Code | Parameter Name | Value | Units | Min Limit | Max Limit |
|----------------|----------------|-------|--------------|-----------|-----------|
| DRNAREA | Drainage Area | 0.43 | square miles | 0.52 | 294 |



Upland Subcat

Indian Run Stream



Routing Diagram for 3287-001-ALLS-HCAD-Stream Study
Prepared by DiPrete Engineering, Printed 1/23/2025
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3287-001-ALLS-HCAD-Stream Study

Prepared by DiPrete Engineering

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Area Listing (all nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|-----------|---------------------------------------|
| 84.568 | 74 | >75% Grass cover, Good, HSG C (1) |
| 28.346 | 98 | Impervious, HSG C (1) |
| 0.743 | 98 | Water Surface, 0% imp, HSG C (1) |
| 68.525 | 70 | Woods, Good, HSG C (1) |
| 93.018 | 77 | Woods, Good, HSG D (1) |
| 275.200 | 77 | TOTAL AREA |

3287-001-ALLS-HCAD-Stream Study

Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 1/23/2025

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Time span=0.00-72.00 hrs, dt=0.01 hrs, 7201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1: Upland Subcat

Runoff Area=275.200 ac 10.30% Impervious Runoff Depth>5.54"
Tc=1,801.0 min CN=77 Runoff=56.42 cfs 127.050 af

Reach 2R: Indian Run Stream

Avg. Flow Depth=1.16' Max Vel=0.70 fps Inflow=56.42 cfs 127.050 af
n=0.100 L=177.1' S=0.0040 '/' Capacity=495.08 cfs Outflow=56.42 cfs 126.999 af

Total Runoff Area = 275.200 ac Runoff Volume = 127.050 af Average Runoff Depth = 5.54"
89.70% Pervious = 246.854 ac 10.30% Impervious = 28.346 ac

3287-001-ALLS-HCAD-Stream Study

Type III 24-hr 100-Year Rainfall=8.50"

Prepared by DiPrete Engineering

Printed 1/23/2025

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Summary for Subcatchment 1: Upland Subcat

Runoff = 56.42 cfs @ 36.02 hrs, Volume= 127.050 af, Depth > 5.54"
 Routed to Reach 2R : Indian Run Stream

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Type III 24-hr 100-Year Rainfall=8.50"

| Area (ac) | CN | Description |
|-----------|----|-------------------------------|
| 68.525 | 70 | Woods, Good, HSG C |
| 28.346 | 98 | Impervious, HSG C |
| 0.743 | 98 | Water Surface, 0% imp, HSG C |
| 93.018 | 77 | Woods, Good, HSG D |
| 84.568 | 74 | >75% Grass cover, Good, HSG C |
| 275.200 | 77 | Weighted Average |
| 246.854 | | 89.70% Pervious Area |
| 28.346 | | 10.30% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---------------|
| 1,801.0 | | | | | Direct Entry, |

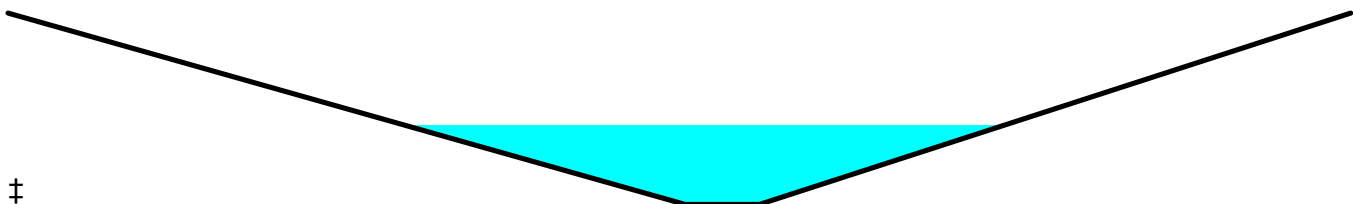
Summary for Reach 2R: Indian Run Stream

Inflow Area = 275.200 ac, 10.30% Impervious, Inflow Depth > 5.54" for 100-Year event
 Inflow = 56.42 cfs @ 36.02 hrs, Volume= 127.050 af
 Outflow = 56.42 cfs @ 36.03 hrs, Volume= 126.999 af, Atten= 0%, Lag= 1.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 Max. Velocity= 0.70 fps, Min. Travel Time= 4.2 min
 Avg. Velocity = 0.50 fps, Avg. Travel Time= 5.9 min

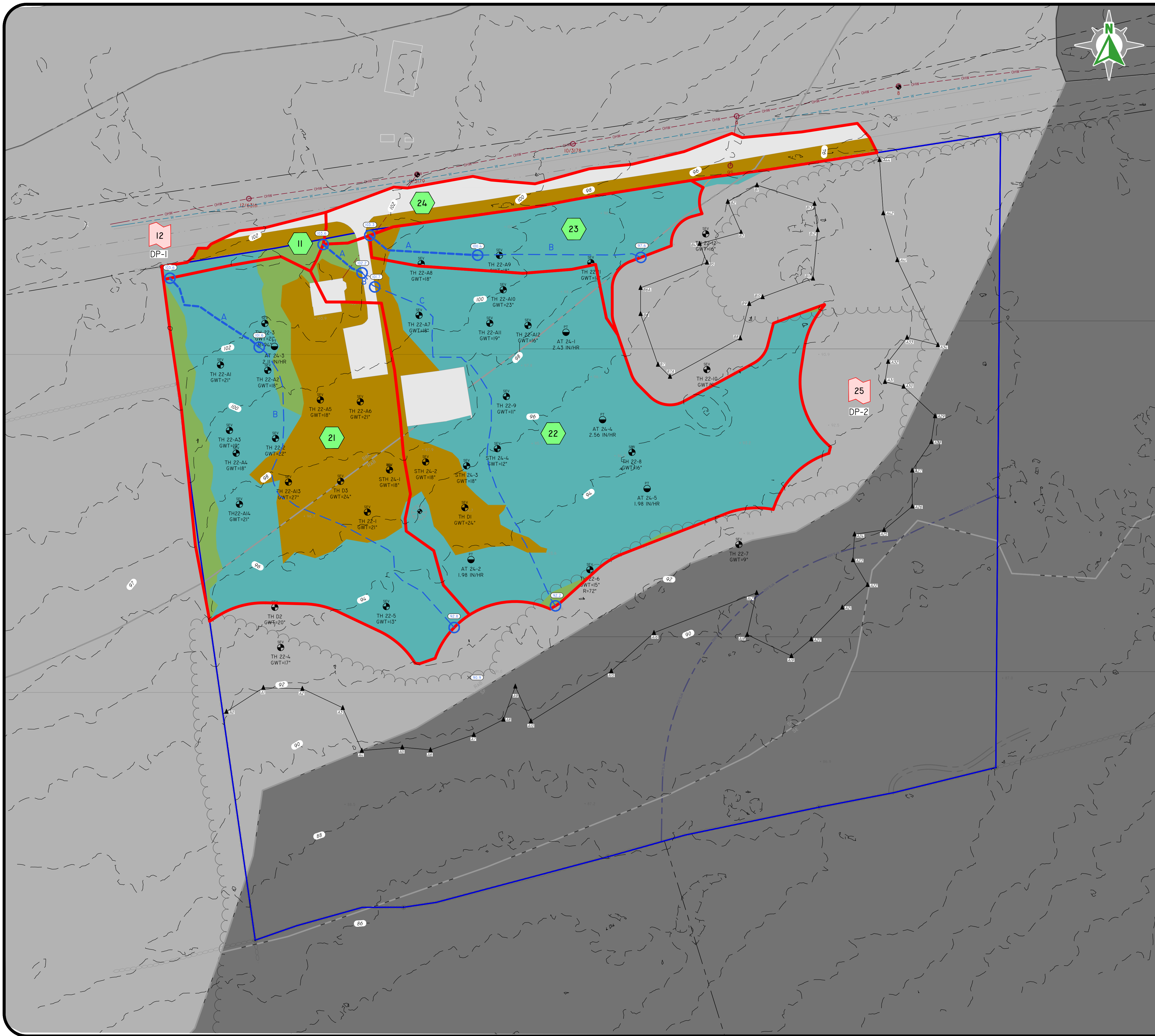
Peak Storage= 14,235 cf @ 36.03 hrs
 Average Depth at Peak Storage= 1.16' , Surface Width= 123.41'
 Bank-Full Depth= 2.80' Flow Area= 408.6 sf, Capacity= 495.08 cfs

15.30' x 2.80' deep channel, n= 0.100
 Side Slope Z-value= 49.8 43.5 ' ' Top Width= 276.54'
 Length= 177.1' Slope= 0.0040 ' '
 Inlet Invert= 87.40', Outlet Invert= 86.70'



Watershed Maps

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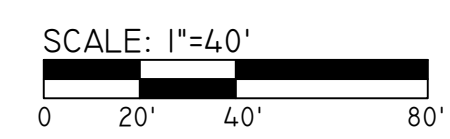


LEGEND

- WOODS - C SOILS
- GRASS - C SOILS
- IMPERVIOUS
- BRUSH - C SOILS

LEGEND

- TC LINE WITH ELEVATIONS
- SUBCATCHMENT AREA
- SOIL BOUNDARY
- REACH
- SUBCATCHMENT
- DESIGN POINT

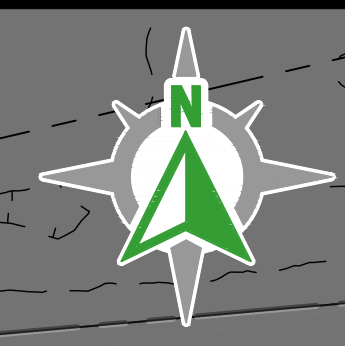
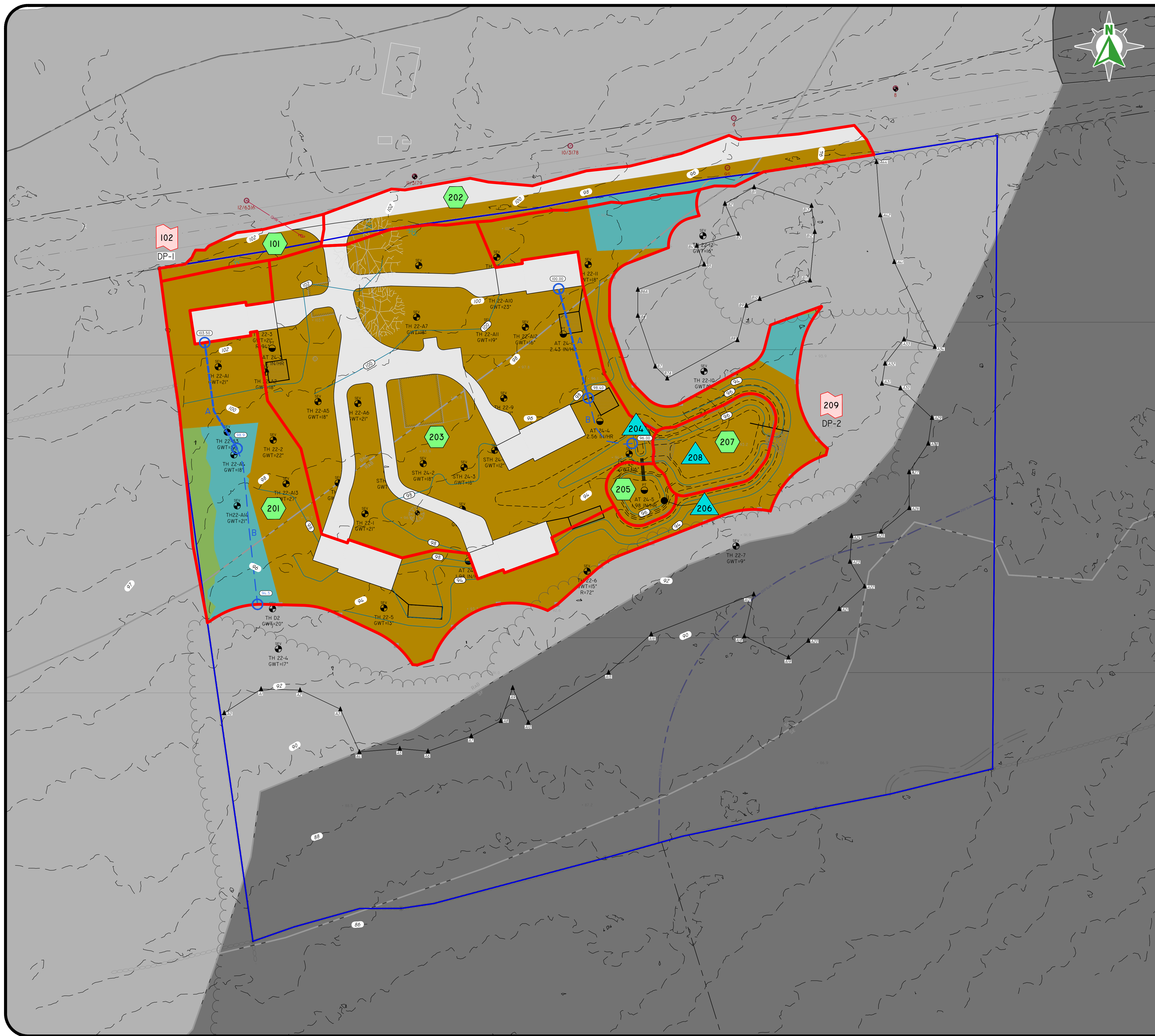


PRE-DEVELOPMENT WATERSHED MAP
SAUGATUCKET ACRES



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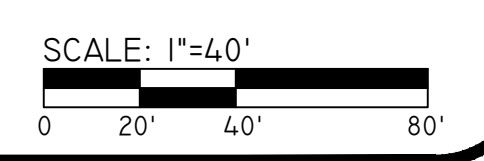


LEGEND

- WOODS - C SOILS [Green box]
- IMPERVIOUS [White box]
- GRASS - C SOILS [Brown box]
- BRUSH - C SOILS [Teal box]

LEGEND

- TC LINE WITH ELEVATIONS [Blue line with circles]
- SUBCATCHMENT AREA [Red line]
- SOIL BOUNDARY [Dashed line]
- REACH [Dashed red line]
- SUBCATCHMENT [Green hexagon]
- DESIGN POINT [Pink hexagon]
- DRAINAGE POND [Teal triangle]



POST-DEVELOPMENT WATERSHED MAP
SAUGATUCKET ACRES



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